

SNYDERS CORNERS  
NORTH  
Bainbridge Twp.

33 Whitney Road - Montville Twp.

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FIELD BOOK

360

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Snyders Corners  
 Northerly T.H. 192  
 Bainbridge Twp

Whitney Road T.H. 65  
 Montville Township Page 33

Whitney Road  
 Location of Westend (1939) Page 55  
 Montville Something (Harold Pison) Pg 99  
 N. Line Bainbridge Twp REF Pg 101

**KEUFFEL & ESSER CO.**  
**DRAWING MATERIALS**  
 AND  
**SURVEYING INSTRUMENTS.**  
**NEW YORK.**

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

**PLEASE RETURN TO**  
 DISTANCES FROM CENTER OF ROADWAY FOR CROSS SECTIONING  
 ROADWAY 48 FEET WIDE SIDE SLOPES 1 TO 1  
**GEAUGA COUNTY ENGINEER**  
 FOR SINGLE TRACK EXCAVATION  
**COURT HOUSE**  
 CHARDON, O. X-14  
**PHONE 250-X**

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.

1  
SNYDER RD. #192 SEC. D-E(pt)  
Align. & drainage structures 3-29 <sup>101</sup>

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WHITNEY RD. #65 SEC. A-B-C  
Align' 33-55  
" relocation Sec. A 55-56  
B.Ms. 63-64  
Cross Sections 66-77

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Snyders Cor. North Road Location

Sta 0+00 Beginning of Imp

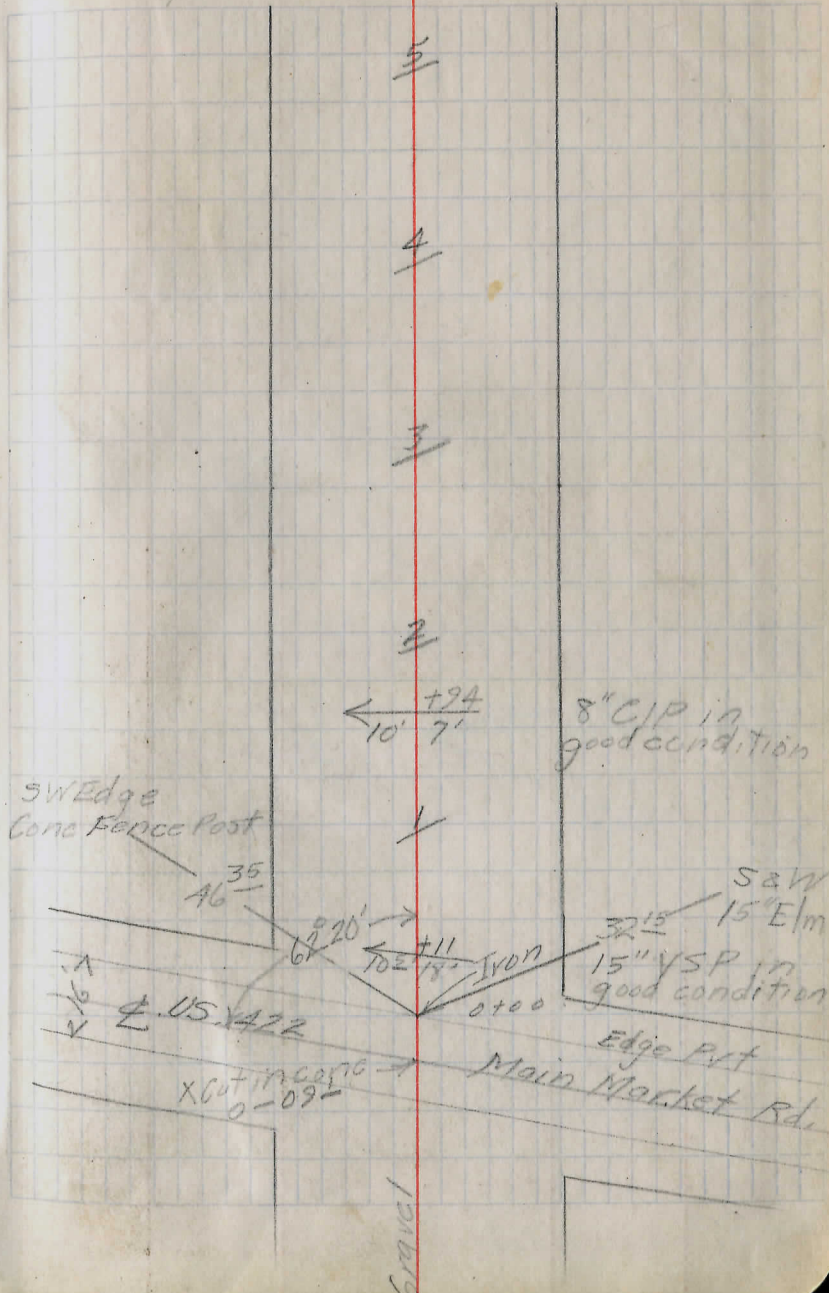
W Edge  
18" Concrete

1928

Archey  
Whistler  
Farris  
Spohn

←  $\frac{+78}{12' 6''}$

12" CIP in 3  
Fair condition.



←  $\frac{+94}{10' 7''}$

8" CIP in  
good condition

SW Edge  
Cone Fence Post

35  
46

8' 20"

←  $\frac{+11}{10' 2 1/2''}$

SW 0700

S&W  
15' Elm

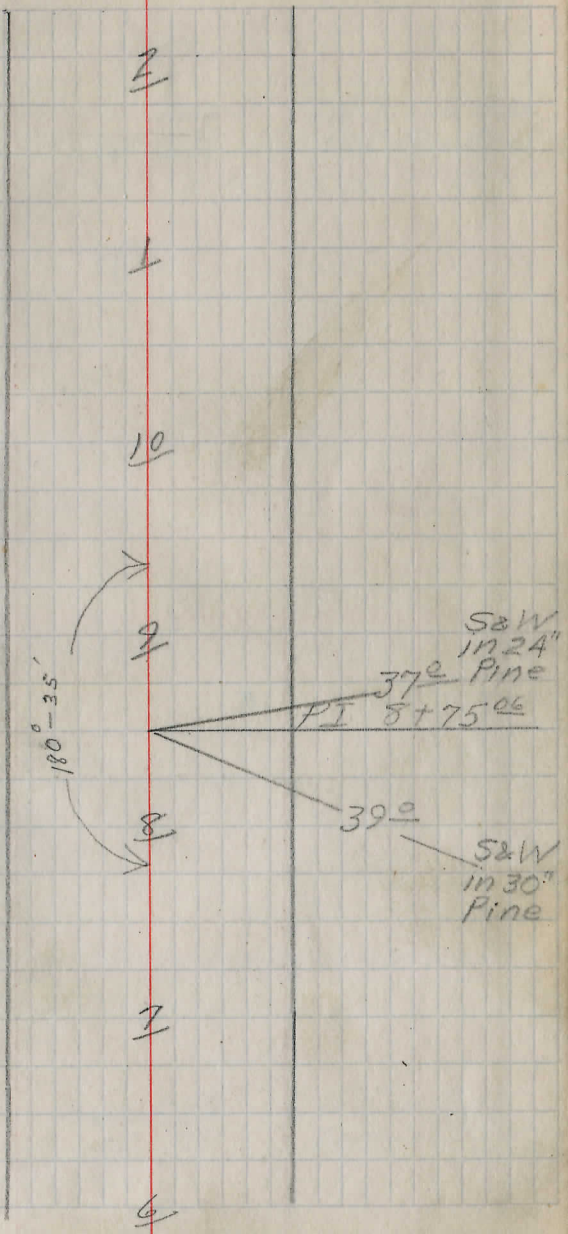
32 1/2  
15" VSP in  
good condition

US 422

X 60' in concrete  
0-09-

Edge Pkt  
Main Market Rd.

Gravel



19

+71.5  
9' 15.5'

old stone Box  
3' x 2' Fair Cond.

18

7

6

15

4

← +46  
3.5 12.8

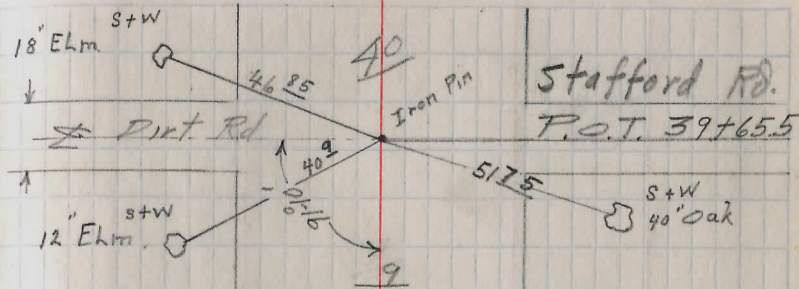
16' Con. Pipe  
Good Condition

13

625432120

32130982

Stafford Rd.



8

7

+45  
11' 5"

8" Corr. Pipe  
Fair Cond.

6

35

+10  
10.5 5.5

8" Corr. Pipe  
Good Cond.

4

2

6

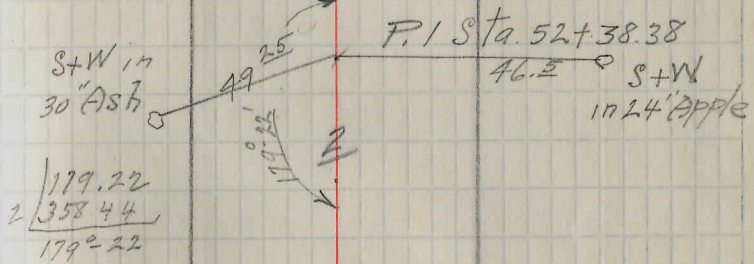
45

4

3

2

1



160222655

(21)

93.85 S+W in  
8" Wild Cherry

POT Sta 68+00

93.86  
S+W in  
8" Elm.

7

6

65

4

3

2

54321709

2

1

80

2

8

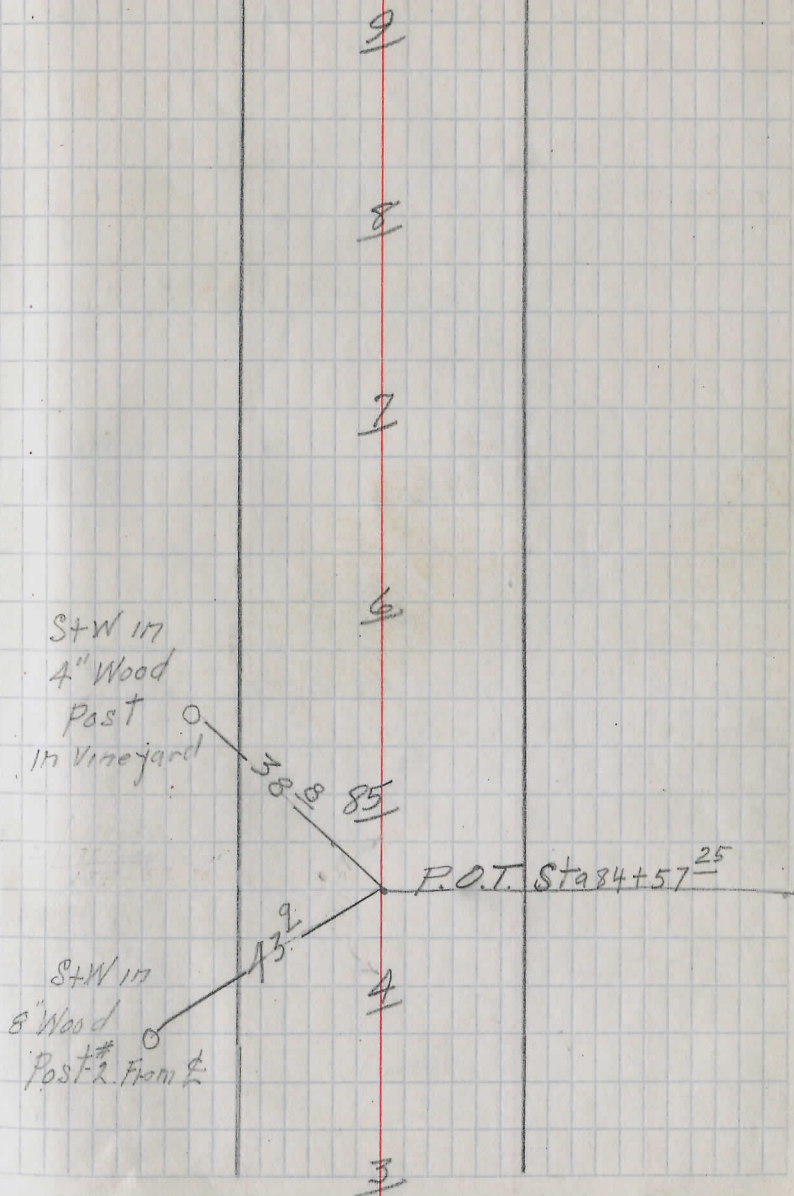
2

—

6

76+15  
Colvert  
Necessary Here

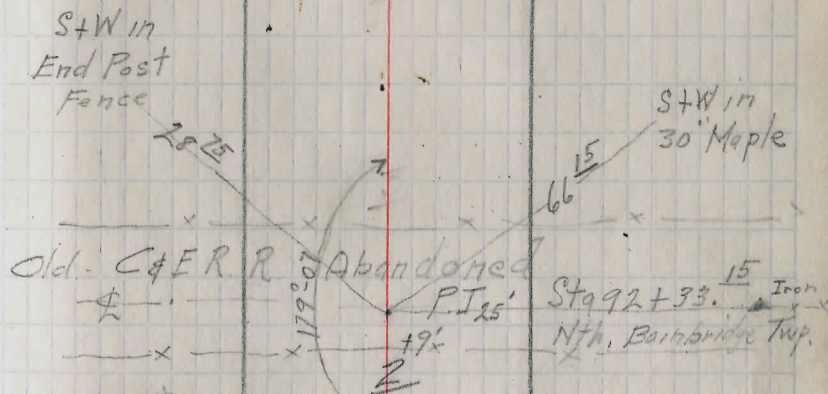
Notes - Whiskyr III - chain      Weather - Rain - Horn  
Parks - 1st.  
Spahn - chain      Clearing - Afternoon  
27



1.75 miles

$$\begin{array}{r} 5280 \overline{) 9233.15} \\ \underline{5280} \\ 39531 \\ \underline{36960} \\ 25715 \end{array}$$

Sta 92+33<sup>15</sup> End of Imp.



44  
1.75 miles

$$\begin{array}{r} 9233 \overline{) 4280} \\ \underline{39531} \\ 36960 \\ \underline{25715} \end{array}$$



Book C-147-Road Records, Geauga County,  
(Montrille Twp.) [Whitney (Rods)]

Beg. at E. line of Montrille Twp. at road laid through  
Harts grove, in Ashland County, about 300 rods  
south of the center of said Twp. - thence S.  $80^{\circ}-45'W$ .

43 chs. 50 links to a post, Thence S.  $88^{\circ}-45'W$ .

1 mile 36 chains 50 links to a line on the Munn  
Tract. Thence S.  $88^{\circ}-45'W$  along said line

2 miles, " continuing the same course

1 mile to the E. line of Hamden Township.

Attest W. W. Beale Surveyor April 29<sup>th</sup> 1834.

Ordered Opened & Recorded December 3<sup>rd</sup> 1834.

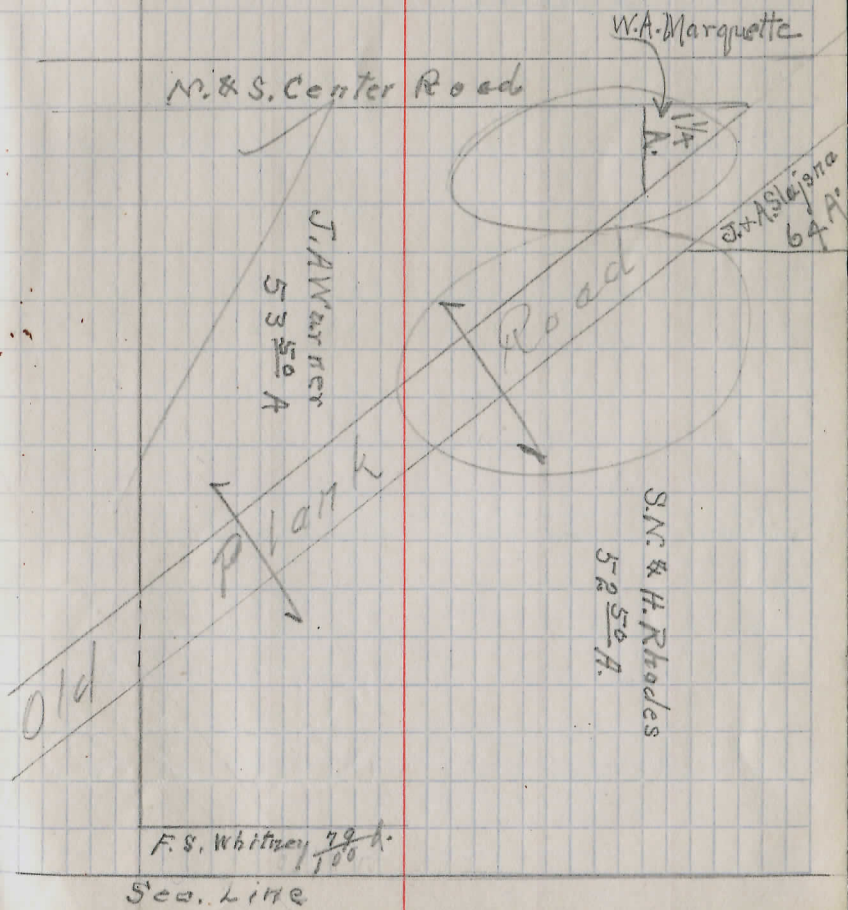
165	43.50 ch	36.56 ch
± 3 rods	66 ft.	66 ft.
4,950.0 ft.	26100	21900
	26100	2,409.0 FT.
	287 1.0 ft.	5 280.01 mi.
		7,689.0 FT.

May. 16<sup>th</sup> 1932 EAF

Sec. Line	J. S. Bodi	Sec. 17	F. S. Whitney	Sec. Line
50	J. Dukot		J. H. Balogh 52 $\frac{54}{4}$	
50A	Wm D. Taylor		P. E. Tolson 50A	
		Let Line	2 $\frac{50}{2}$	
57 $\frac{59}{4}$	Marie Taylor		Thuman 48 $\frac{50}{4}$	
57 $\frac{59}{4}$	H. A. Reiser		W 48 $\frac{50}{4}$	

Ashtabula County -  
Hartsquare Township.





AL

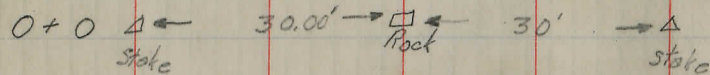
3662.314'  
3262.438'

# Whitney Road Location

2+51.5

2+0

1+0



R.P. stakes set by Ashtabula Co.  
Surveyors.

May. 20, 1932  
Clear & warm

E.A. Fiedler 43  
H. Borton  
S. Merritt

8+0

7+0

6+0

5+0

4+0

3+0

q. of bridge  
+51.5

2+0

1+0

Geengo  
County  
Fence  
(County Line)  
Ashtabula  
County

M. 51.5  
586.15 W

81°56'

7°55'

Note:- Offset  
stakes set at 30'  
on Rt. every 500'.  
Others set at  
20' except on  
plowed fields = Lt.

18+ 57.25 P.O.T.

19+0

+57.25

18+0

17+0

16+0

15+0

Marie Taylor

14+0

+14.25 FL  
Fence →

13+0

12+0 H. & A. P. Taylor

11+0

10+0

9+0

spike  
Co. P.O.T.

Hub  
Δ

29+0

+ 06

28+0

27+0

26+0

25+0

+ 74.0

24+0

23+0

"

+ 41

22+0

21+0

20+0

P. &amp; E. Patchin


P.L.

Wire Fence →

Truman M. E. Elroy

(P.L.?)

Wire Fence →


 Plank Collect.  
About 8" x 12"

May 21, 1932  
Fair & Warm

E.A. Fiedler  
H. Barton  
S. Merritt

46

+10

Wire Fence

40+0

39+0

38+0

37+0

36+0

35+0

34+0

33+0

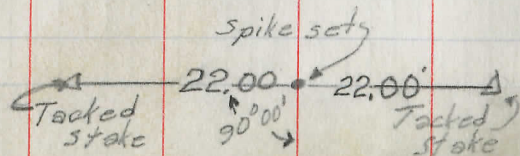
32+0

31+0

30+0

29+ 91.71

187° 58' 15"  
P.I.



€

54+0

Whitney

+ 30

Approx. W. line of  
J. Bologh

53+0

52+0

51+0

+ 055 P.O.T

Spike  
set

50+0

49+0

48+0

W. side of House.

47+0

Plank Sluice

+ 47.40 P.O.T.

Spike  
set

42+0

41+0

40+30.8

Wire Fence ↗

△ ← 1500ft →  
Hub

Vant Spk N rout  
16" Evergreen  
(1st E of dr)

6033

Spk E side  
CEI 566 937

2915

Spk NE side  
20" Evergreen  
(Most Easterly)

3820

I Pipe fd & re ref.  
4/26/59 Mostly cloudy  
warm windy

4/26/59  
5756.60  
to 486

48

+54<sup>00</sup> P.O.T.

Spk Set (5-21-52) g.w.  
(3/4" iron pipe set 8' below  
surface of roadway  
5-23-32)

66+0

65+0

64+0

63+0

62+0

61+0

60+0

59+0

58+0

57+0

56+0

55+0

May 23, 1932  
Clear & Warm

E. A. Fiedler  
H. Barton  
S. Merritt

49

79+0

J. & I. Bodi

A. M. Forinacci

78+0

+37

+4.20 + +0.25

Stone bridge with  
conc. top. & parapets  
9' opening.

77+0

76+0

75+0

74+0

73+0

72+0

71+0

70+0

+93

— Pipe

69+0

+11.5

68+0

1 1/2 ft  
H.S.B.

67+0

89+6462

Δ ← 80 8944 →  
H46

92+0

91+0 P. Brown

90+0

+64.60 P.O.T.

Spike Set

89+0

88+25 P.L.

Whitney

88+0

+15±

P.L.

+01

87+0

1/2 sty.  
Fr. Hse.

Sandor

86+0

85+0

84+0

+05

83+0

Fr. School  
Hse.

Ethel C.

82+0

Kamorczy

A. & E. Sandor

81+0

+40±

P.L.

80+0

Probable 1st line

4/25/59  
2295.82 → 4.8.86  
Ref. B.55

Spk N side  
Tele pole

0

58.36

Spk NE side  
10" Apple

3

48.89

Nail E side  
CEI

0

29.62

4/25/59  
boat spk fd POT  
(No indication that  
point is of Sun rd)

105+0

104+0

P. Brown

103+0

102+0

101+0

100+0

+152 d Rd South → Sun Rd

99+0

98+0

97+0

96+0

+85

10 = O Big Rock  
Springs both sides.

95+0

94+0

93+0

115+56<sup>90</sup>

P.O.T.

Hole in Sandstone

93.98

106+04<sup>12</sup>

P.O.T.

Spike Set

3 tacks N. root  
24" Pine

22.00 ft.

34.00 ft.

3 tacks W. root  
12" Maple

117+0

116+0

+56<sup>90</sup> P.O.T.

Hole in Sandstone  
(ledge Rock)

115+0

114+0

113+0

J.A. Warner

112+0

111+0

110+0

S. N. & H. Rhodes

109+0

108+0

+80.7

5.2 11.9 small stone slice  
stone parapets

107+0

106+44

P.L.

106+04<sup>12</sup>

F.S. Whitney

Spike Set P.L.

Wire Fence P.L.

Wire Fence

Sec. line.

106+0

P. Brown

F.S. Whitney

123+45<sup>23</sup> P.O.T.  $\Delta$  10<sup>20ft</sup>  $\rightarrow$  Spike Set  
Hub

1

123+45<sup>23</sup> P.O.T. Spike Set

122+0

121+0

120+0

119+0

118+0

N-85°30'W

133+88

Nail in Stake W. Margin N.&S.  
ctr. Rd. by corner post.

133+37 P.O.T.

Nail  
Set

133+58 ± 2 of N.&amp;S. ctr. Rd.

132+79 W. side of house 31.5 So. of 4.

130+91

E. side of barn 30' S. of 4.

129+37

Low place for sluice.

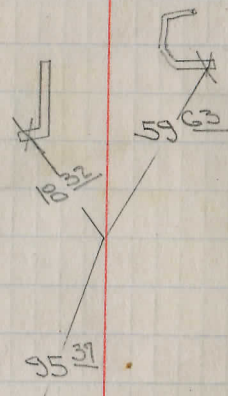
# Relocation of Whitney

5/19/39 Fair - Warm  
Pomeoy - Clouse - Willman

$2+23^{35} = 174+32^{55}$   
 $\rightarrow 75^{00}$   
 C.E. pole # 560408

X in E end Hdw

$0+0 = 122+09^{20}$



X in N.W. end of Hdw

Set W in N.E.

Root 14" W Cherry

95.00

106+04<sup>12</sup>

# Road (West end) May '39

N 80° W

P.O.T. Spike (set)

139-46  
279-32

Spike set from R.P. Sta

Warren Road  
S.H. 153

P.O.T. I. Bolt (set)

156+03<sup>60</sup> S.H. 153

Painesville  
Center of Culdt

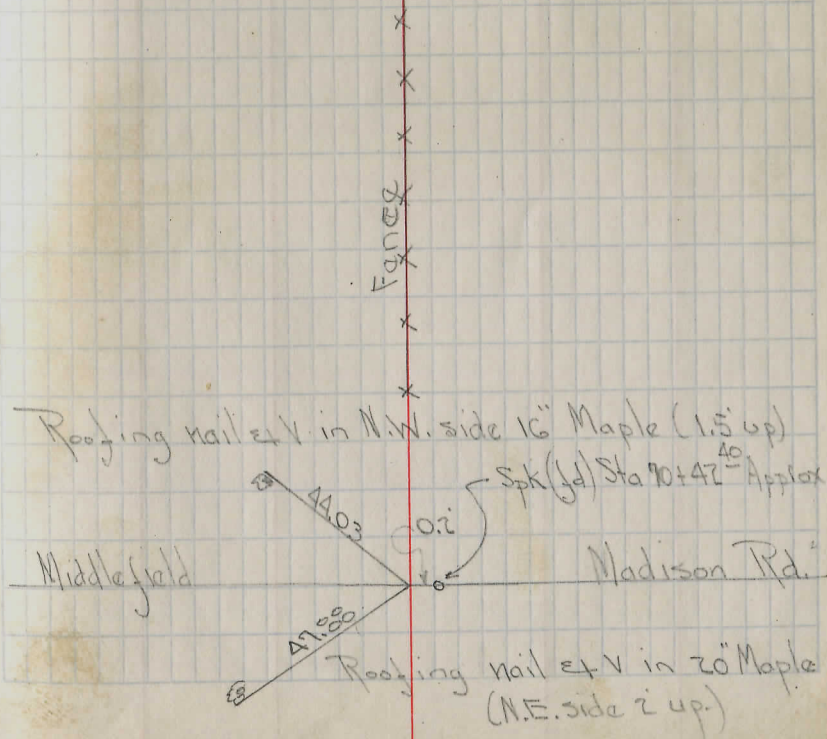
Spike found & checked from R.P.

Note: Line established by juggling between  
Sta. 106+04<sup>12</sup> & center of X post of fence  
line running west from N & S. Center Rd.

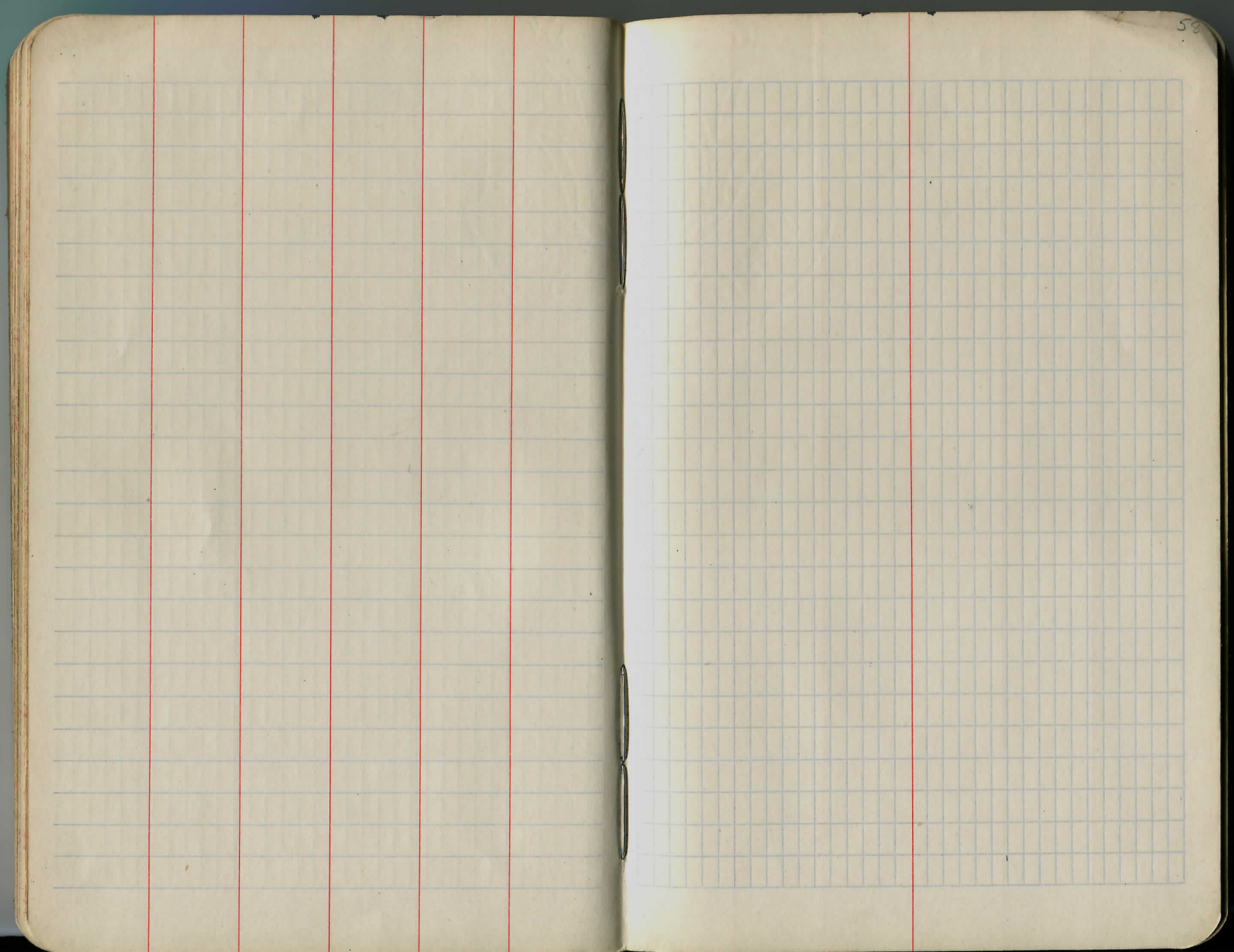
Stakes set 30' Rt.

11+50<sup>9.00</sup>  
= 133+60<sup>18</sup>

Bolt (set)

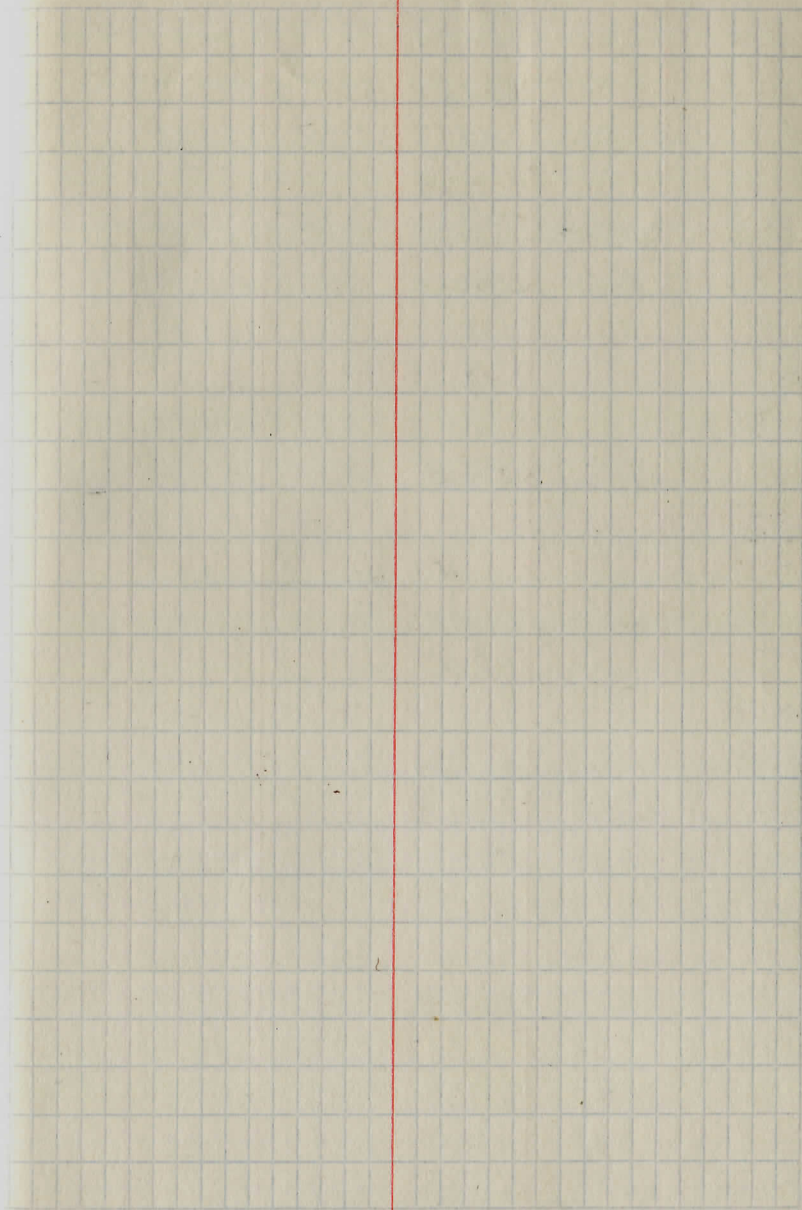
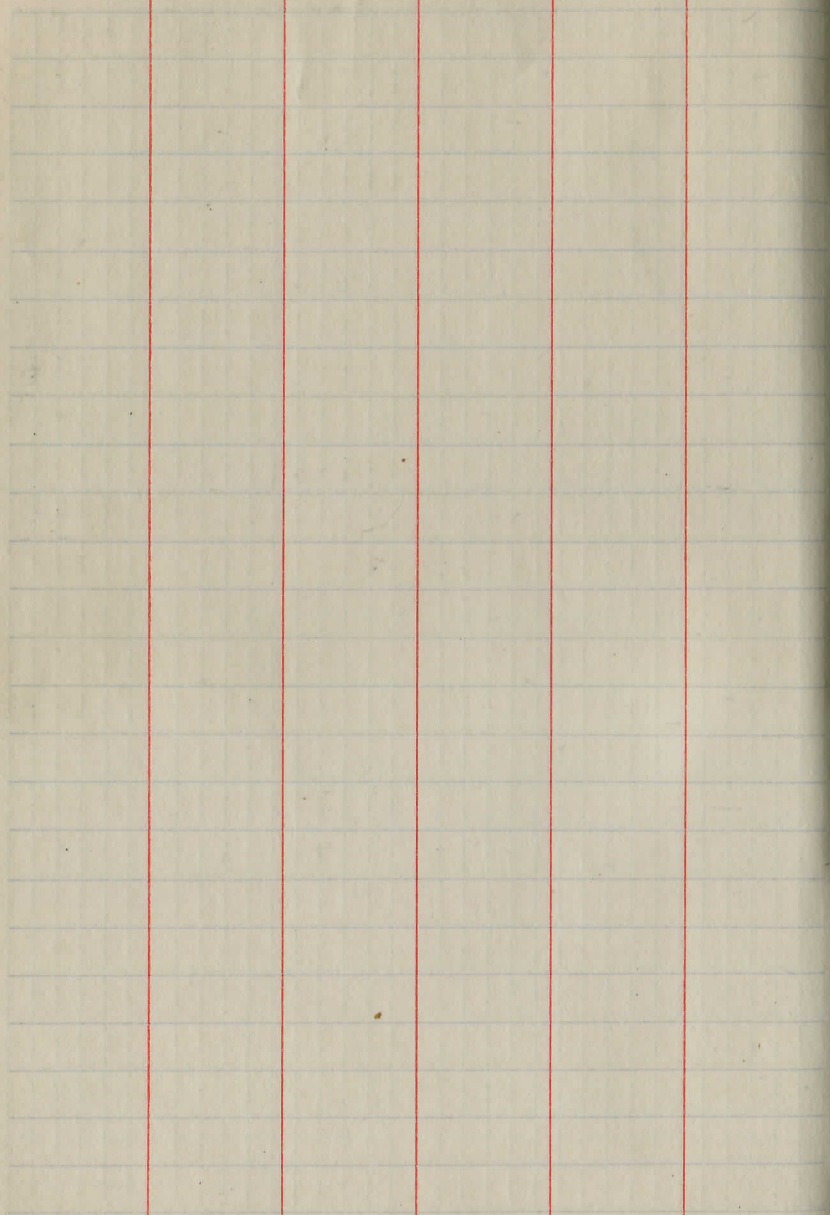


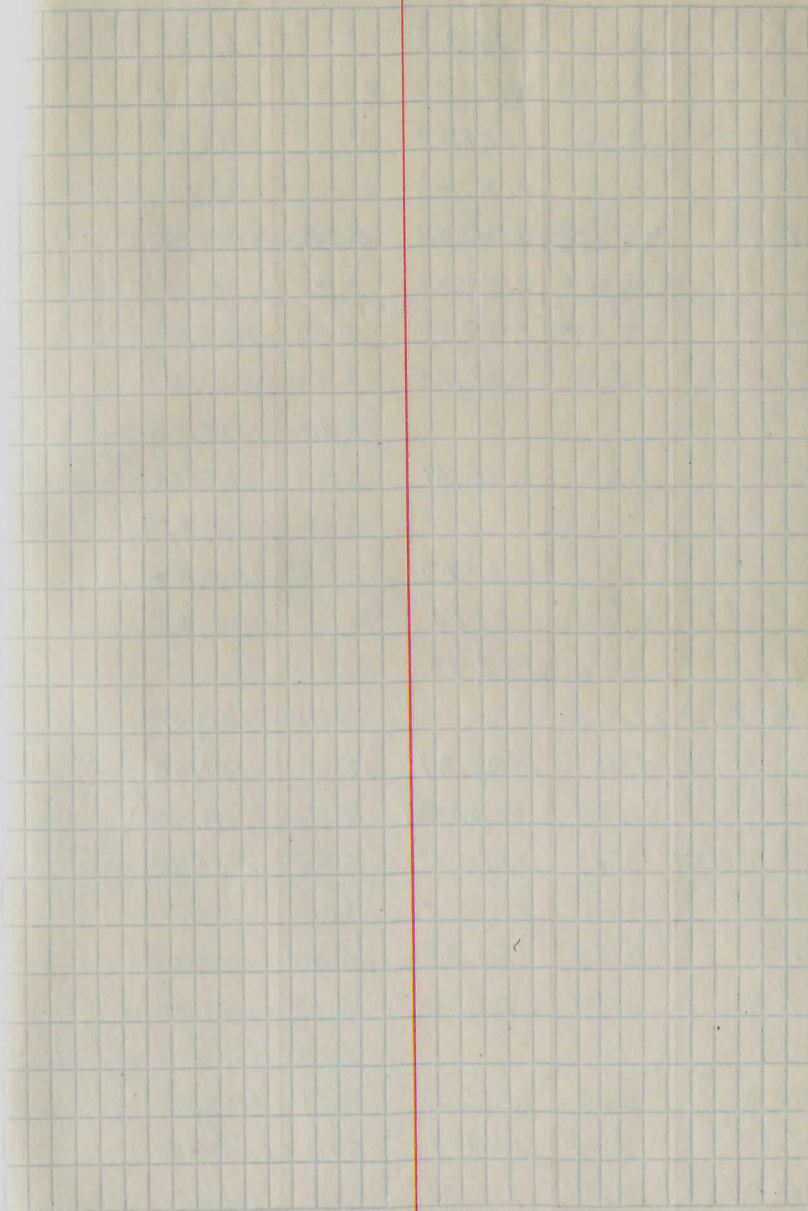






The image shows an open notebook with two pages. The left page is ruled with horizontal lines and has four vertical red margin lines. The right page is ruled with horizontal lines and has a large grid area with a vertical red margin line on the left side. The number '60' is written in the top right corner of the right page.





May 24, 1932  
Clear & Warm

H. Barton  
S. Merritt

		H.I.	-	Elev.
B.M.	2.12	1144.94		1142.82
T.P.	4.38	1145.07	4.23	1140.71
T.P.	2.34	1141.69	5.74	1139.35
T.P.	0.93	1139.86	2.74	1138.93
T.P.	7.08	1143.18	4.74	1135.10
T.P.	2.99	1139.26	5.91	1136.27
T.P.	3.89	1139.59	3.54	1135.70
T.P.	5.15	1141.15	3.59	1136.00
B.M.			2.40	1138.75
T.P.	1.35	1136.51	5.99	1135.16
T.P.			7.16	1129.35
T.P.	7.75	1137.13	-7.25	1129.85
T.P.	2.29	1132.14	-2.19	1129.95
	2.98	1132.93		
B.M.			2.36	1130.57
T.P.	4.46	1126.34	11.05	1121.88
T.P.	1.78	1120.46	7.64	1118.68
B.M. & T.P.	5.14	1120.77	4.85	1115.61
T.P.	2.43	1118.14	5.06	1115.71
T.P.	5.58	1117.83	5.89	1112.25
T.P.	6.59	1122.29	2.13	1115.70
B.M.			3.10	1112.19
T.P.	2.80	1116.76	8.33	1113.96
T.P.	3.88	1114.54	6.10	1110.66
B.M. & T.P.	3.55	1113.97	4.12	1110.42

Terris.  
Spike in F.  
root 26"  
Maple 85  
L<sup>+</sup> Sta 114.2  
Old Plank Rd

Spike in S.W.  
of S.W. Corner  
Fr. School Hse  
30' Lt. Sta  
Sta. 83+05  
(Spike about  
1 1/2' above  
ground)

Spike in N.W.  
root 10' Erugon  
25' Lt. Sta  
26+30  
(Also T.P.  
spike)

Spike in S. side  
8' Elm. 25' Lt.  
Sta 54+40

Spike in N. side  
8' Erugon  
30' Lt. Sta.  
43+40

Spike in W. road  
8' Elm 40' Lt.  
Sta. 31+40

Whitney Rd - Mont.  
F.C.P.

B.M. #8

B.M. #7

B.M. #6

B.M. #5

B.M. #4

1113.97

	+	H.I	-	Elev.	Remarks
T.P.	2.88	1110.91	5.94	1108.03	
B.M. & T.P.	1.90	1110.92	2.39	1108.52	spike in NW side 12" Apple 40' Sta 20+20
T.P.	3.47	1105.44	8.65	1101.77	
T.P.	3.91	1102.57	6.78	1098.66	
B.M.			3.63	1098.94	spike S.W. side 14" Apple 35' Rt. Sta. 9+40
T.P.	2.73	1098.04	7.24	1095.31	
T.P.	7.45	1098.42	7.07	1090.97	
B.M.			1.12	1097.30	spike in S. foot 24" Maple = 20' Rt. Sta. 0+45
{ B.M. #1 Transferred 2 1/2' South 100' E. of Co. Line }	+2.452	1099.75	-3.061	1096.69	(Probably a R.R. spike set by Ash-tabula Co. Surveyors)
	+1.85	1098.54	13.30	1085.24	
B.M. #8	3.73	1142.48		1138.75	
T.P.	6.15	1145.73	2.90	1139.58	
T.P.	9.09	1152.86	1.96	1143.77	
T.P.	11.26	1161.97	2.15	1150.71	
B.M. #9			1.51	1160.46	spike in S. side 15" Walnut, 6" above ground 20' Rt. Sta. 101+25
B.M. #10				1186.28	spike N.W. Root 10" Maple 27' Rt. Sta 109+40 Elev.
B.M. #11				1214.79	X - in Lodge Rock 40' Rt Sta. 115+60 Elev.
B.M. #12				1243.19	spike in W. Root 12" wild cherry 25' Lt Sta 121+15 Elev.

B.M. #3

B.M. #2

B.M. #1

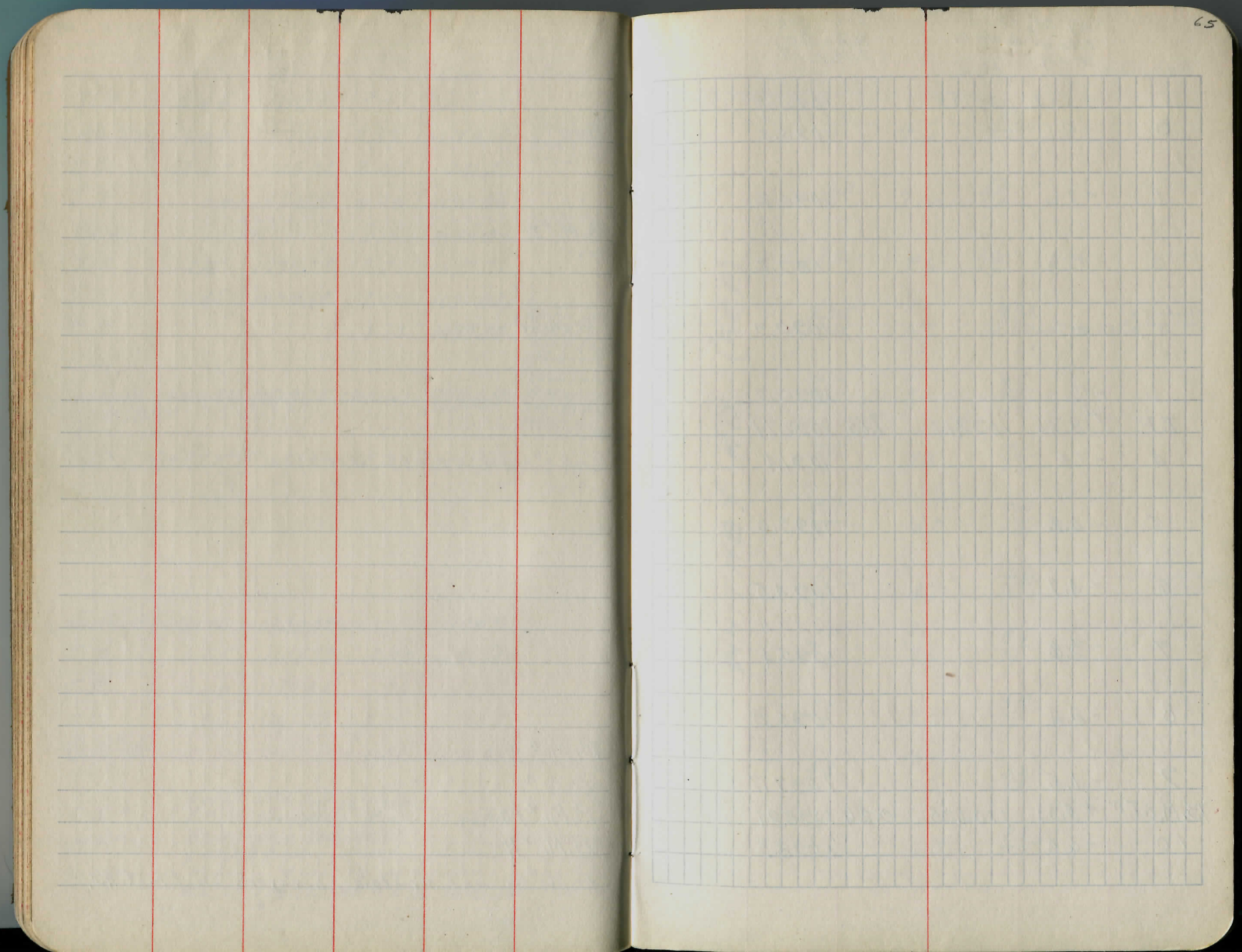
Ft. Red. of creek water 6" deep, outlet of "Monticello Pitch."

B.M. #9

B.M. #10

B.M. #11

B.M. #12 Set by State Surveyors on Plank Rd.



May 25, 1932  
Clear & warm  
Windy. H I

E. A. Fiedler,  
H. Barton,  
S. Merritt

Rainier P.M.

	+1.15	1097.54		1096.69
0	-4.6			1093.2
1	-7.6			1090.2
2	-8.6			1089.2
Bridge 51.5	-6.9			1090.9
3	-7.1			1090.7
T.P.	+8.44	1099.17	7.13	1090.71
4	-7.8			1091.4
5	-6.2			1093.0
6	-4.7			1094.5
7	-3.8			1095.4
8	-2.4			1096.8
9	-1.5			1097.7
B.M. & T.P.	+5.34	1104.25	0.24	1098.91
10	-6.0			1098.3

Rec. Elev  
1098.94

LT

RT

66

WHITNEY RD. (F.C.P.)

$\frac{5.2}{9}$	4.6	$\frac{5.3}{7.8}$
$\frac{5.0}{5}$	7.6	$\frac{8.6}{7.3}$
$\frac{9.6}{9}$	8.6	$\frac{9.5}{7.5}$
$\frac{8.45}{\text{Top. Hgt.}}$	6.9	$\frac{9.90}{\text{bed, stream no water}}$
$\frac{8.5}{8.5}$	7.1	$\frac{8.6}{7.3}$
$\frac{9.0}{10}$	7.8	$\frac{9.0}{7.4}$
$\frac{7.7}{11}$	6.2	$\frac{7.4}{7.2}$
$\frac{5.9}{11}$	4.7	$\frac{6.2}{7.1}$
$\frac{4.7}{12}$	3.8	$\frac{5.0}{7.1}$
$\frac{3.8}{12}$	2.4	$\frac{3.9}{7.2}$
$\frac{2.9}{11}$	1.5	$\frac{3.2}{7.2}$
$\frac{7.6}{10}$	6.0	$\frac{7.5}{7.3}$

		1104.25		
11	-5.6			1098.7
12	-5.0			1099.3
13	-4.1			1100.2
14	-2.9			1101.4
15	-2.2			1102.1
T.P.	+6.44	1109.49	1.40	1102.85
16	-7.1			1102.4
17	-6.2			1103.3
18	-4.4			1105.1
19	-2.8			1106.7
20	-2.9			1106.6
B.M. & T.P.	+1.77	1110.26	1.00	1108.49
21	-4.3			1106.0
22	-4.5			1105.8
22+41	-4.1			1106.2

Rec. Elev.  
1108.52

Plank Sluice Flow N.E.

Lt	E	Rt
$\frac{7.2}{11}$	5.6	$\frac{6.9}{12}$
$\frac{6.4}{11}$	5.0	$\frac{6.2}{12}$
$\frac{5.1}{10}$	4.1	$\frac{5.1}{12}$
$\frac{4.4}{10}$	2.9	$\frac{4.2}{11}$
$\frac{3.8}{10}$	2.2	$\frac{3.6}{11}$
$\frac{8.5}{11}$	7.1	$\frac{8.4}{11}$
$\frac{7.3}{11}$	6.2	$\frac{7.4}{11}$
$\frac{5.4}{10}$	4.4	$\frac{5.4}{10}$
$\frac{4.4}{9}$	2.8	$\frac{4.2}{11}$
$\frac{8.5}{10}$	2.9	$\frac{4.1}{10}$
$\frac{5.2}{9}$	4.3	$\frac{5.4}{9}$
$\frac{5.5}{10}$	4.5	$\frac{5.6}{10}$
$\frac{4.3}{10}$	4.1	$\frac{5.7}{10}$

1104.6 1105.0 1102.6  
3.6  
100 200 300  
6.3 7.7 8.7

		1110.26		
23	- 4.2			1106.1
24	- 3.7			1106.6
25	- 2.7			1107.6
T.P.	+ 6.23	1113.55	2.94	1107.32
26	- 5.4			1108.2
27	- 5.0			1108.6
28	- 4.0			1109.6
29	- 4.6			1109.0
29+33	- 4.2	Plank S/wice		1109.4
30	- 4.7			1108.9
31	- 4.1			1109.5
B.M.&T.P.	+ 3.37	1113.75	3.17	1110.38
32	- 3.5			1110.3
33	- 3.7			1110.1
33+54	- 4.0			1109.8
		10" Cor. I.P. Culvert	Flow S. about	
		70' ft. thence S.E. about 150' thence	Ely.	
34+0	- 4.1			1109.7

Rec. Elev. 1110.42

grade to 1107.44 f.p.e.

$$\begin{array}{r} 24 \quad 4 \quad R+ \\ \hline 5.3 \\ 77 \end{array} \quad \begin{array}{r} 4.2 \\ \hline \end{array} \quad \begin{array}{r} 5.3 \\ 8 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline 77 \end{array} \quad \begin{array}{r} 3.7 \\ \hline \end{array} \quad \begin{array}{r} 4.7 \\ 7 \end{array}$$

$$\begin{array}{r} 3.4 \\ \hline 73 \end{array} \quad \begin{array}{r} 2.7 \\ \hline \end{array} \quad \begin{array}{r} 3.7 \\ 6 \end{array}$$

$$\begin{array}{r} 6.4 \\ \hline 75 \end{array} \quad \begin{array}{r} 5.4 \\ \hline \end{array} \quad \begin{array}{r} 6.7 \\ 4 \end{array}$$

$$\begin{array}{r} 6.0 \\ \hline 77 \end{array} \quad \begin{array}{r} 5.9 \\ 7.0 \end{array} \quad \begin{array}{r} 5.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ \hline 21 \end{array} \quad \begin{array}{r} 4.9 \\ 4.0 \end{array} \quad \begin{array}{r} 4.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ \hline 16 \end{array} \quad \begin{array}{r} 4.6 \\ 4.2 \end{array} \quad \begin{array}{r} 5.4 \\ 3 \end{array}$$

$$\begin{array}{r} 5.3 \\ \hline 6 \end{array} \quad \begin{array}{r} 4.7 \\ \hline \end{array} \quad \begin{array}{r} 5.4 \\ 13 \end{array}$$

$$\begin{array}{r} 5.1 \\ \hline 6 \end{array} \quad \begin{array}{r} 4.1 \\ \hline \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 9 \end{array} \quad \begin{array}{r} 3.5 \\ \hline \end{array} \quad \begin{array}{r} 4.3 \\ 11 \end{array}$$

$$\begin{array}{r} 5.1 \\ \hline 7 \end{array} \quad \begin{array}{r} 3.7 \\ \hline \end{array} \quad \begin{array}{r} 4.7 \\ 10 \end{array}$$

$$\begin{array}{r} 8.5 \\ 430 \end{array} \quad \begin{array}{r} 4.5 \\ 80 \end{array} \quad \begin{array}{r} 110.0 \\ 70 \end{array} \quad \begin{array}{r} 6.0 \\ 5 \end{array} \quad \begin{array}{r} 4.0 \\ \hline \end{array} \quad \begin{array}{r} 5.7 \\ 11 \end{array}$$

$$\begin{array}{r} 6.5 \\ \hline 12 \end{array} \quad \begin{array}{r} 4.1 \\ \hline \end{array} \quad \begin{array}{r} 5.7 \\ 11 \end{array}$$

		1113.75		Elev.	
35	-4.1			1109.7	
35+40	-3.3			1110.5	
				Plank Slice 5' opening Flows into S. ditch. Then E to ditch at 33+54	
36	-3.4			1110.4	
37	-2.8			1111.0	
T.P.	+7.12	1118.01	2.86	1119.89	
38	-6.1			1111.9	
39	-5.2			1112.8	
40	-4.5			1113.5	
41	-3.5			1114.5	
42	-1.2			1116.8	
T.P.	+4.52	1122.38	2.15	1115.86	
42+47	-4.4			1118.0	
43	-5.8			1116.6	
B.M. #5			3.26	1119.12	Rec. Elev. 1119.19
44	-8.2			1114.2	
45	-9.2			1113.2	

$$\frac{6.0}{11} \quad \text{\$} \quad 4.1 \quad \frac{7.7}{9}$$

$$\frac{6.0}{10} \quad 3.3 \quad \frac{6.2}{10}$$

$$\frac{4.4}{12} \quad 3.4 \quad \frac{4.4}{7}$$

$$\frac{3.4}{13} \quad 2.8 \quad \frac{3.5}{6}$$

$$\frac{7.1}{13} \quad 6.1 \quad \frac{6.8}{5}$$

$$\frac{6.2}{14} \quad 5.2 \quad \frac{6.0}{6}$$

$$\frac{5.6}{15} \quad 4.5 \quad \frac{5.4}{5}$$

$$\frac{4.5}{13} \quad 3.5 \quad \frac{4.0}{6}$$

$$\frac{2.1}{12} \quad 1.2 \quad \frac{1.9}{6}$$

$$\frac{5.2}{11} \quad 4.4 \quad \frac{5.4}{8}$$

$$\frac{6.1}{9} \quad 5.8 \quad \frac{6.4}{5}$$

$$\frac{9.4}{9} \quad 8.2 \quad \frac{9.0}{10}$$

110.8 Pond  
75' water l deep

$$\frac{10.8}{13} \quad 9.2 \quad \frac{10.3}{11}$$

		1122.38		
T.P.	+4.17	1116.98	9.57	1112.81
46	-4.2			1112.8
47	-4.0			1111.0
47+56	-4.4	Plant sluice	Flow N.E. ly.	1112.6
48	-5.1			1111.9
49	-5.1			1111.9
50	-3.2			1113.8
T.P.	+4.94	1120.49	1.45	1115.53
50+75	-4.1			1116.4
51	-4.0			1116.5
52	-4.8			1115.7
53	-5.0			1115.5
54	-4.8			1115.7
T.P.	+4.76	1120.53	4.72	1115.77
B.M. #6			4.99	1115.52
	+4.99	1120.60		1115.61

Rec. Elev.  
1115.61

Rec. Elev.

Lt.		Rt.
$\frac{5.0}{14}$	42	$\frac{4.9}{3}$
$\frac{6.0}{19}$	5.1	$\frac{5.8}{2}$
$\frac{6.2}{17}$	4.4	$\frac{1110.3}{6.7} \frac{6.3}{160} \frac{6.4}{260} \frac{6.7}{300} \frac{6.9}{400}$
$\frac{6.4}{19}$	5.1	$\frac{6.1}{3}$
$\frac{6.2}{21}$	5.1	$\frac{6.1}{4}$
$\frac{4.5}{18}$	3.2	$\frac{1111.5}{5.2} \frac{6}{6}$
$\frac{5.8}{15}$	4.1	$\frac{1113.2}{7.3} \frac{7}{7}$
$\frac{5.6}{15}$	4.0	$\frac{7.2}{7}$
$\frac{6.5}{15}$	4.8	$\frac{6.7}{8}$
$\frac{6.0}{16}$	5.0	$\frac{7.0}{6}$
$\frac{6.1}{15}$	4.8	<del><math>\frac{6.8}{6}</math></del>

		1120.60		
54+60	- 5.7			1114.9
55	- 4.8			1115.8
56	- 4.5			1116.1
57	- 3.7			1116.9
58	- 2.8			1117.8
T.P.	+ 9.06	1126.23	3.43	1117.17
59	- 4.7			1119.5
60	- 4.7			1121.5
61	- 4.5			1121.7
62	- 4.1			1121.8
63	- 3.2			1123.0
T.P.	9.69	1131.91	4.01	1122.22
64	- 8.1			1123.8
65	- 6.3			1125.6
66	- 3.0			1128.9

E.I. of Water  
in SW corner  
at sta 54+

Lt.	±	Rt.
$\frac{5.7}{15}$	4.8	$\frac{6.3}{5}$
$\frac{5.2}{10}$	4.5	$\frac{5.2}{4}$
$\frac{4.7}{15}$	3.7	$\frac{4.7}{4}$
$\frac{3.8}{13}$	2.8	$\frac{3.8}{4}$
$\frac{8.0}{10}$	6.7	$\frac{7.7}{7}$
$\frac{6.6}{7}$	4.7	$\frac{6.2}{3}$
$\frac{5.6}{9}$	4.5	$\frac{5.6}{7}$
$\frac{5.4}{10}$	4.4	$\frac{5.5}{7}$
$\frac{4.6}{10}$	3.2	$\frac{4.6}{8}$
$\frac{9.2}{8}$	8.1	$\frac{9.0}{9}$
$\frac{7.2}{6}$	6.3	$\frac{7.0}{8}$
$\frac{3.8}{8}$	3.0	$\frac{4.1}{10}$

#7		1131.91			
73.M.&T.P.	+2.85	1133.42	1.34	1130.57	Rec. Elev. 1130.57
66+54	-3.4			1130.0	
67	-3.5			1129.9	
68	-4.8			1128.6	
69	-5.9			1127.5	
69+95	-5.8	10012" Cor. Pipe		1127.6	1220.67
70	-6.0			1127.4	
T.P.	+7.38	1134.91	5.89	1127.53	
71	-6.9			1128.0	
72	-5.5			1129.4	
73	-4.3			1130.6	
74	-2.5			1132.4	
T.P.	+3.18	1135.81	2.28	1132.63	
75	-4.8			1131.0	
76	-6.4			1129.4	
T.P.					

Lt.	£	Rt.
$\frac{4.6}{8}$	3.4	$\frac{4.5}{11}$
$\frac{4.8}{9}$	3.5	$\frac{4.9}{11}$
$\frac{5.6}{9}$	4.8	$\frac{5.9}{9}$
$\frac{7.0}{11}$	5.9	$\frac{7.2}{9}$
$\frac{7.35}{400}$ $\frac{11.24}{300}$ $\frac{9.6}{200}$ $\frac{8.2}{100}$ $\frac{7.5}{14}$	5.8	$\frac{7.4}{7}$
$\frac{7.4}{14}$	6.0	$\frac{7.3}{7}$
$\frac{8.0}{12}$	6.9	$\frac{8.0}{9}$
$\frac{7.0}{9}$	5.5	$\frac{7.1}{10}$
$\frac{5.0}{8}$	4.3	$\frac{5.1}{10}$
$\frac{3.6}{9}$	2.5	$\frac{3.9}{11}$
$\frac{5.9}{8}$	4.8	$\frac{6.0}{14}$
$\frac{7.1}{8}$	6.4	$\frac{7.2}{14}$

May 24, 1932  
Clear & warm

E. A. Fiedler  
H. Barten  
S. Merritt

1135.81

77 -5.7

T.P.

77+37

4.4

Stone bridge with conc. top  
and parapets.

+6.25 1138.60

78 -7.5

79 -6.7

80 -5.6

81 -4.7

82 -3.8

83 -2.7

T.P. +5.28 1142.78

B.M.

+4.05 1142.80

84 -5.5

85 -4.4

86 -3.9

1130.1

3.44 1132.35

1131.4

1132.35

1131.1

1131.9

1133.0

1133.9

1134.8

1135.9

1.10 1137.50

4.05 1138.73

1138.75

1137.3

1138.4

1138.9

S.E. Cor. of  
S. Parapet  
of conc.  
culvert  
Sta 77+37

Rec. Elev.  
1138.75

Rec. Elev.  
Used.

Lt.

C

Rt.

$\frac{7.3}{10}$

5.7

$\frac{7.5}{13}$

$\frac{7.4}{10}$

1128.4

1126.2 1127.1 1127.1 1127.5

$\frac{7.4}{10+13}$

4.4

$\frac{7.6}{13}$

$\frac{1124.2}{5.00}$

$\frac{8.3}{9}$

7.5

$\frac{8.5}{11}$

$\frac{7.9}{10}$

6.7

$\frac{7.8}{11}$

$\frac{7.3}{10}$

5.6

$\frac{7.5}{11}$

$\frac{6.2}{10}$

4.7

$\frac{6.5}{10}$

$\frac{5.2}{10}$

3.8

$\frac{5.1}{10}$

$\frac{4.0}{11}$

2.7

$\frac{4.4}{11}$

$\frac{7.1}{10}$

5.5

$\frac{7.2}{11}$

$\frac{6.4}{10}$

4.4

$\frac{6.1}{12}$

$\frac{136.4}{6.0}$

$\frac{6.0}{11}$

3.9

$\frac{5.3}{12}$

		1142.80		
87	-3.2			1139.6
88	-2.3			1140.5
T.P.	+5.95	1146.07	2.68	1140.12
88+07		Drainage South		
89	-5.1			1141.0
90	-4.5			1141.6
91	-3.8			1142.3
92	-2.5			1143.6
93	-1.1			1145.0
T.P.	+9.74	1154.53	1.28	1144.79
94	-8.5			1146.0
95	-6.7			1147.8
96	-4.7			1149.8
97	-2.8			1151.7
98	-0.4			1154.1

culvert  
1139.0  
2-12' culvert

4.9	4	7.4
12	3.2	4.4
1137.9		11
1138.6		
4.2	2.3	3.7
11		10
1136.8		
1137.5		
1138.2		
1138.7		
1138.5		
9.3		
400	300	200
74	74	76
100	11	
6.9	5.1	6.3
11		11
6.6	4.5	5.6
11		11
5.7	3.8	5.0
10		12
4.5	2.5	3.7
10		10
3.2	1.1	2.7
9		11
10.5	8.5	10.1
9		13
8.3	6.7	8.2
7		13
5.4	4.7	5.7
9		13
3.8	2.8	4.1
10		11
1.7	0.4	2.1
9		9



		1178.32		
T.P.	+10.43	1188.41	0.34	1177.98
109	-9.4			1179.0
B.M. #10			1.43	1186.98
110	-3.2			1185.2
T.P.	+12.67	1200.71	0.37	1188.04
111	-11.2			1189.5
112	-6.9			1193.8
113	-3.0			1197.7
T.P.	12.74	1213.27	0.18	1200.53
114	-8.6			1204.7
115	-1.4			1211.9
T.P.	+11.31	1223.96	0.62	1212.65
B.M. #11			9.17	1214.79
115+42 <sup>2</sup>	-8.6			1215.4
115+57	-6.2			1217.8
115+93	-3.8			1220.2
116	-3.7			1220.3
T.P.	+11.44	1234.25	1.15	1222.81
117	-9.2			1225.1

Spike NW  
10" Maple 20"  
Rt. Sta 103+  
40

Stone 115+10

X in ledge  
Rock 40 ft  
Rt. Sta 115+60

(From Sta 115+42 to Sta  
115+93 Ledge Rock out-  
crop.)

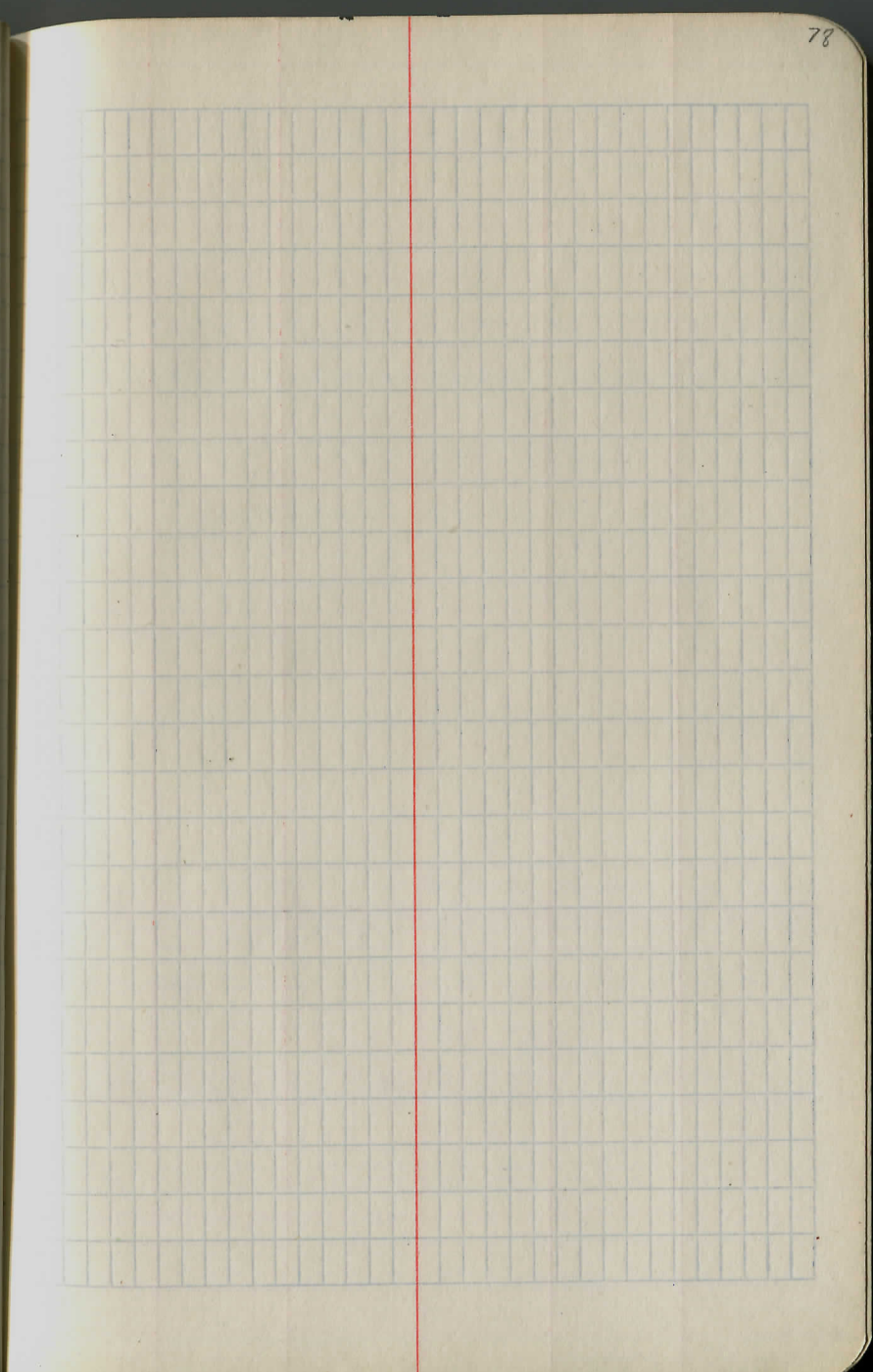
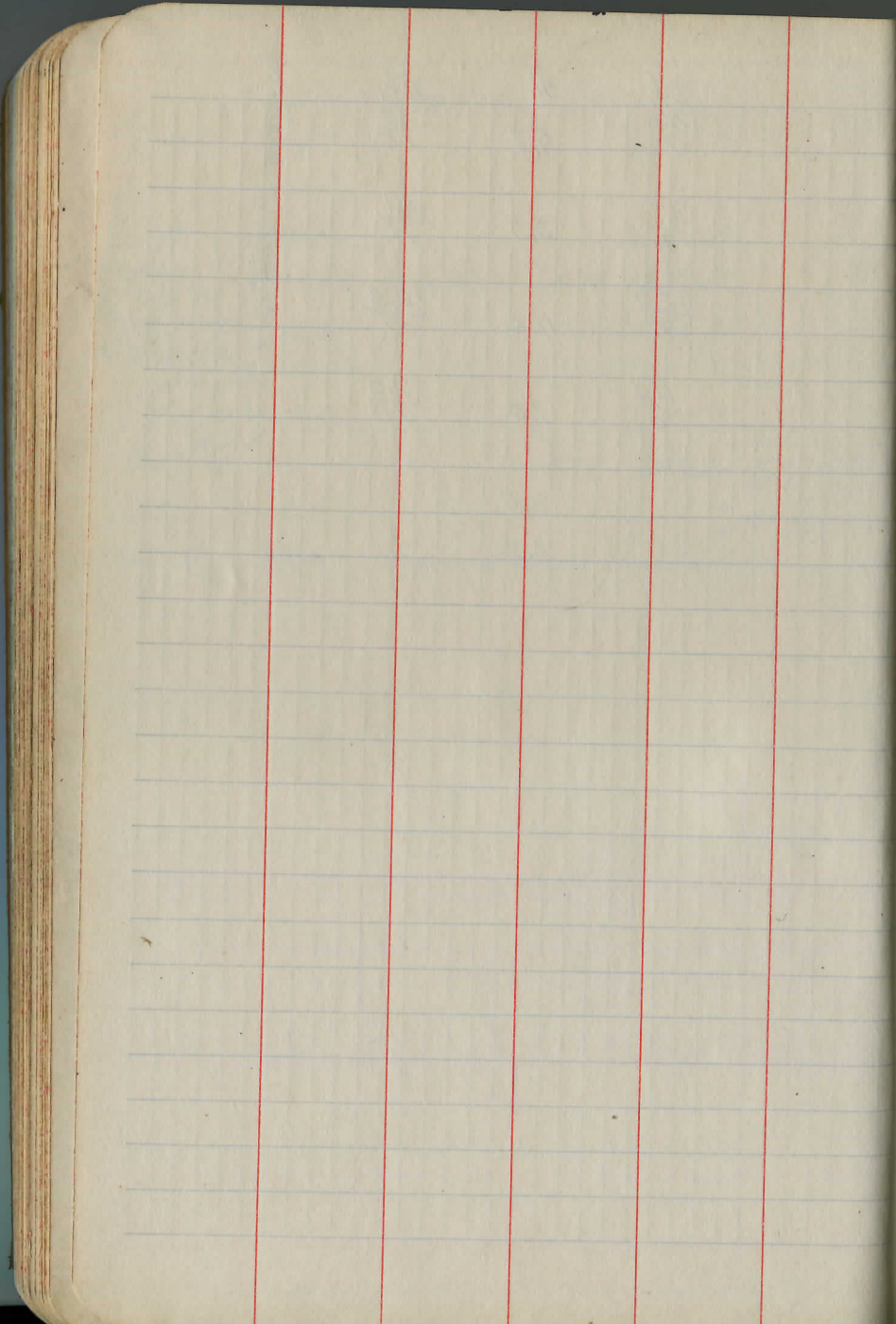
Lt.	¢	Rt.
$\frac{10.3}{5}$	9.4	$\frac{10.1}{10}$
$\frac{4.5}{6}$	3.2	$\frac{4.7}{11}$
$\frac{12.5}{8}$	11.2	$\frac{12.5}{11}$
$\frac{7.7}{14}$	6.9	$\frac{7.4}{3}$
$\frac{3.3}{20}$	$\frac{3.1}{5}$	3.0
$\frac{11.3}{16}$	$\frac{10.0}{3}$	8.6
$\frac{2.1}{15}$	$\frac{2.0}{1}$	1.4
$\frac{8.6}{18}$	$\frac{8.2}{7}$ Rock	8.6
$\frac{6.5}{15}$ Rock	6.2 Rock	$\frac{6.7}{3}$ Rock
$\frac{4.7}{11}$	$\frac{3.8}{5}$ Rock	3.8 Rock
$\frac{4.3}{11}$	3.7	$\frac{4.4}{6}$
$\frac{10.4}{6}$	9.2	$\frac{10.3}{11}$

$\frac{12.2}{9}$   $\frac{10.0}{20}$  Approx

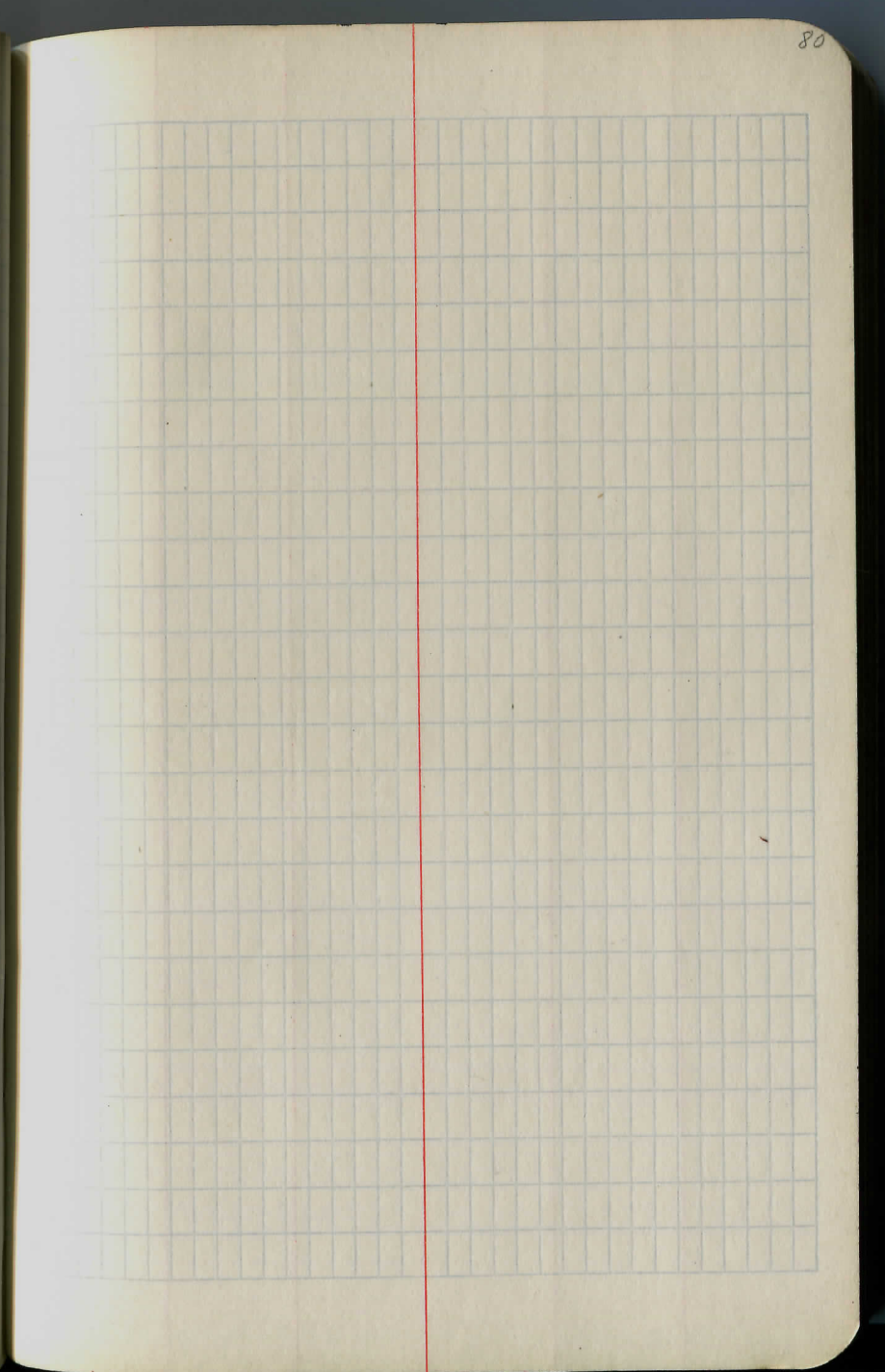
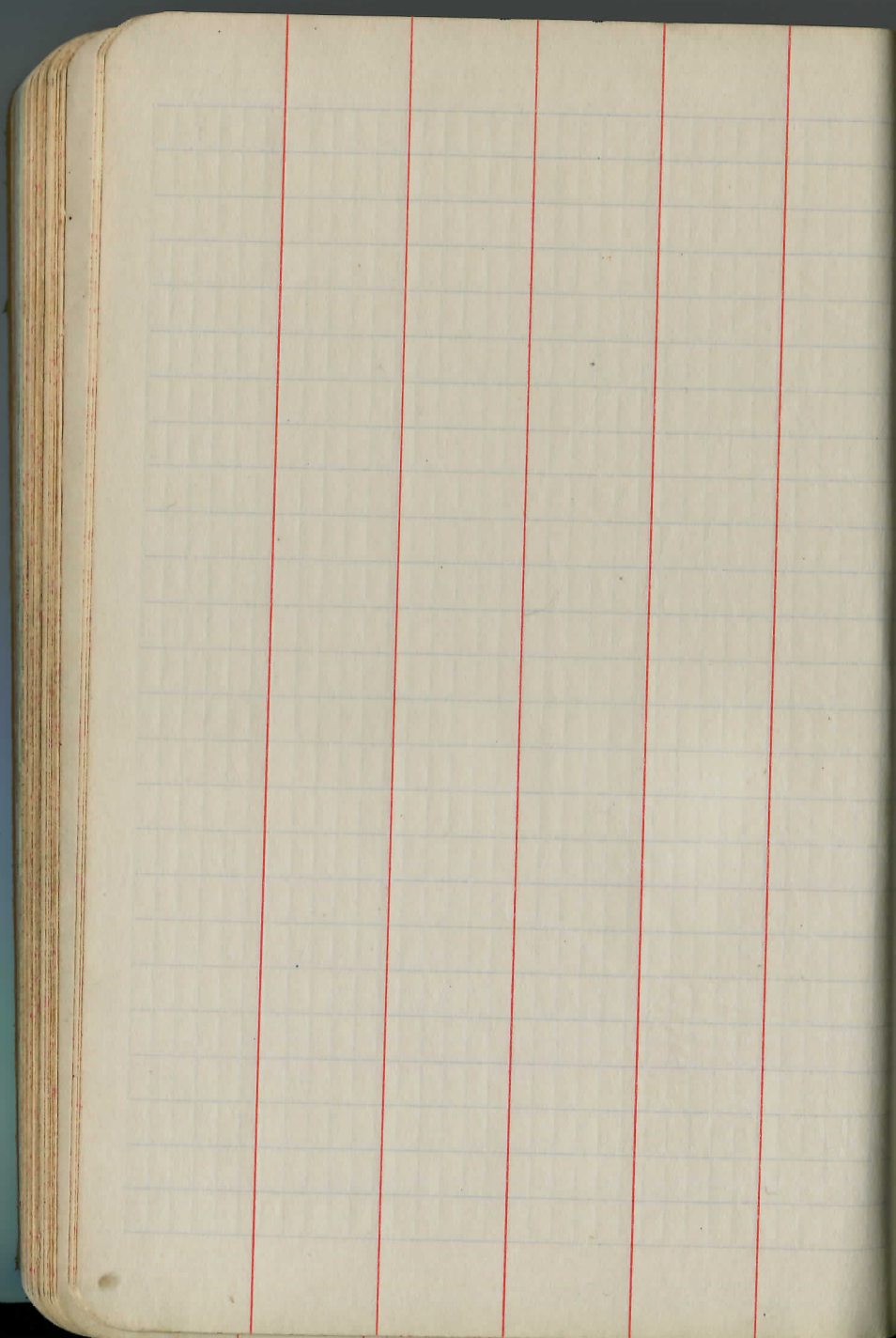
$\frac{4.8}{13}$   $\frac{12.8}{30}$

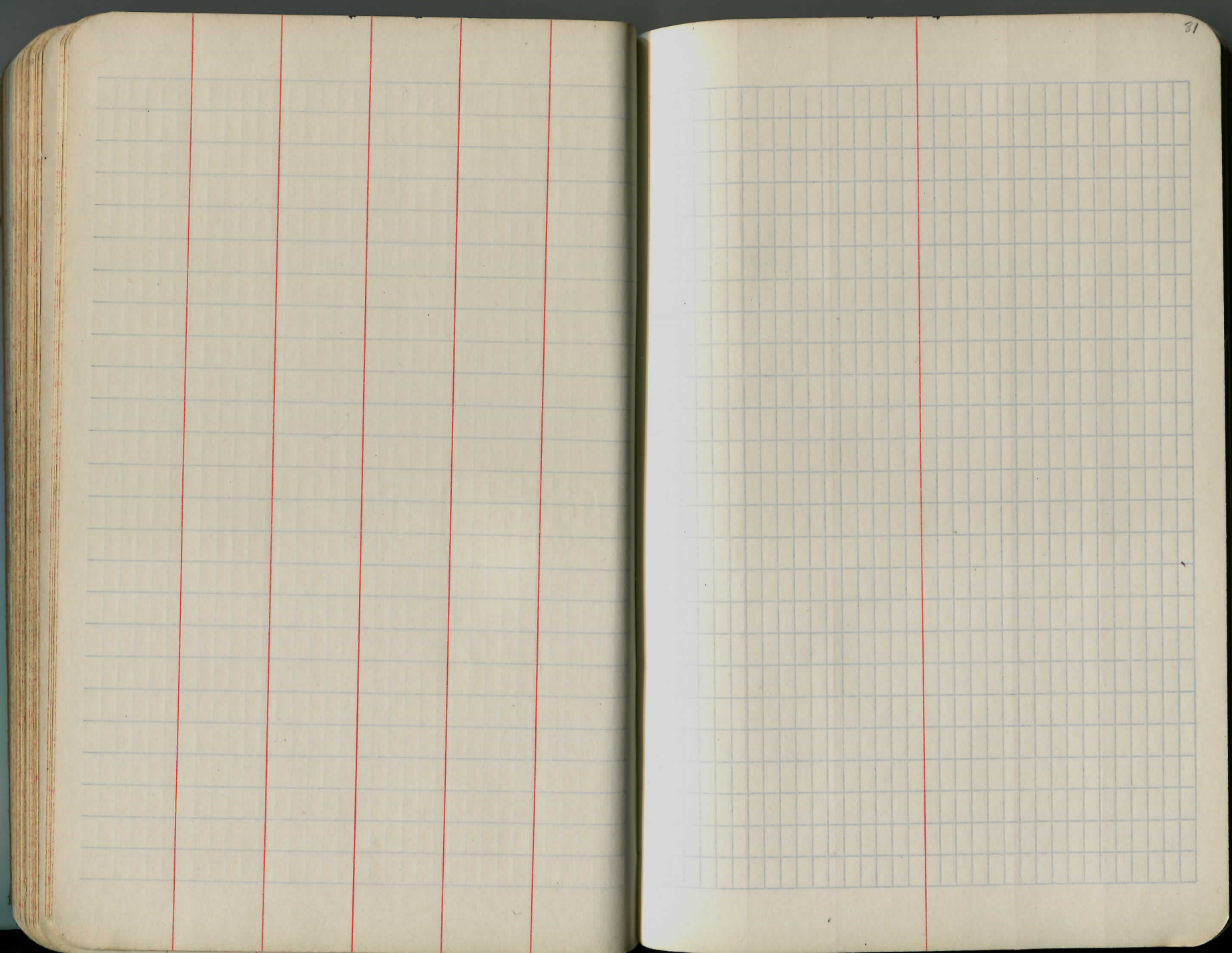
$\frac{10.9}{7}$  More or less level to 20

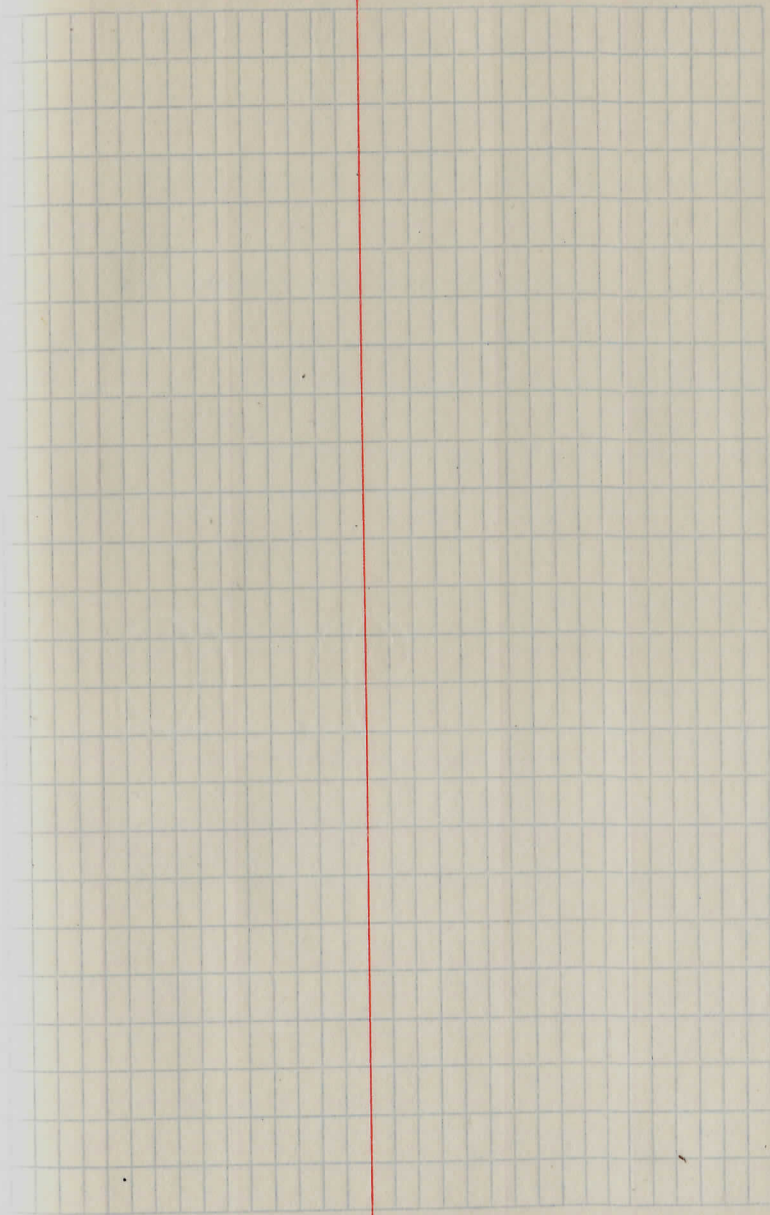
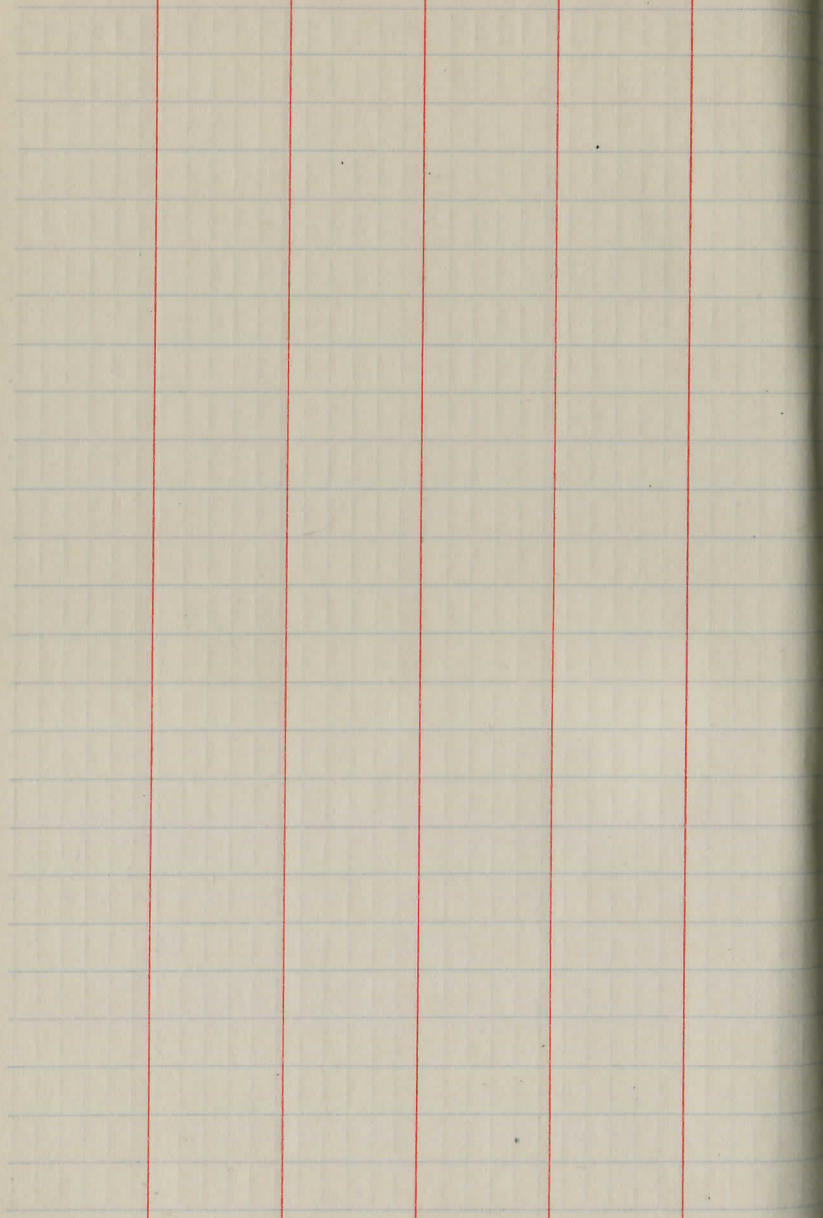


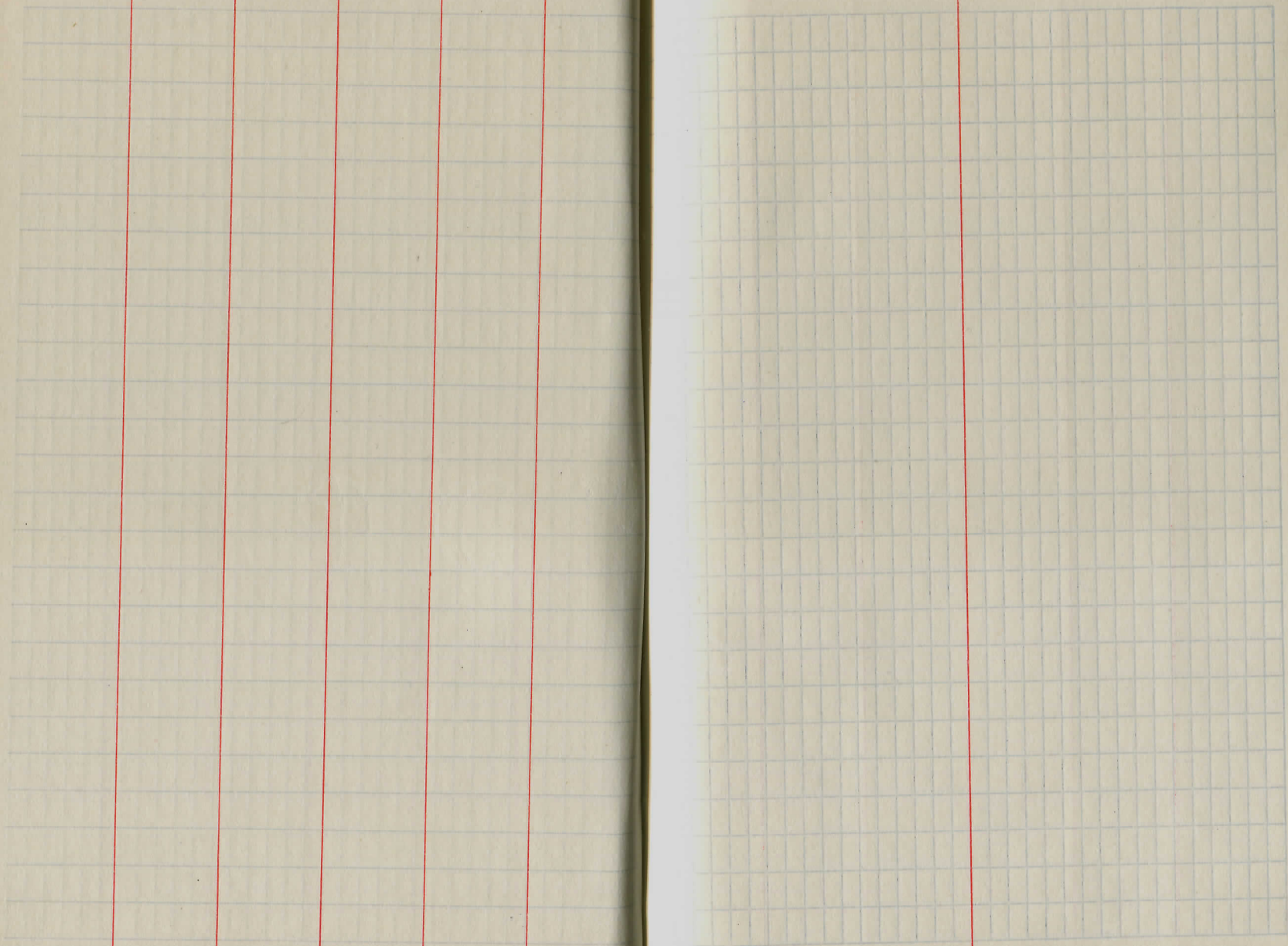


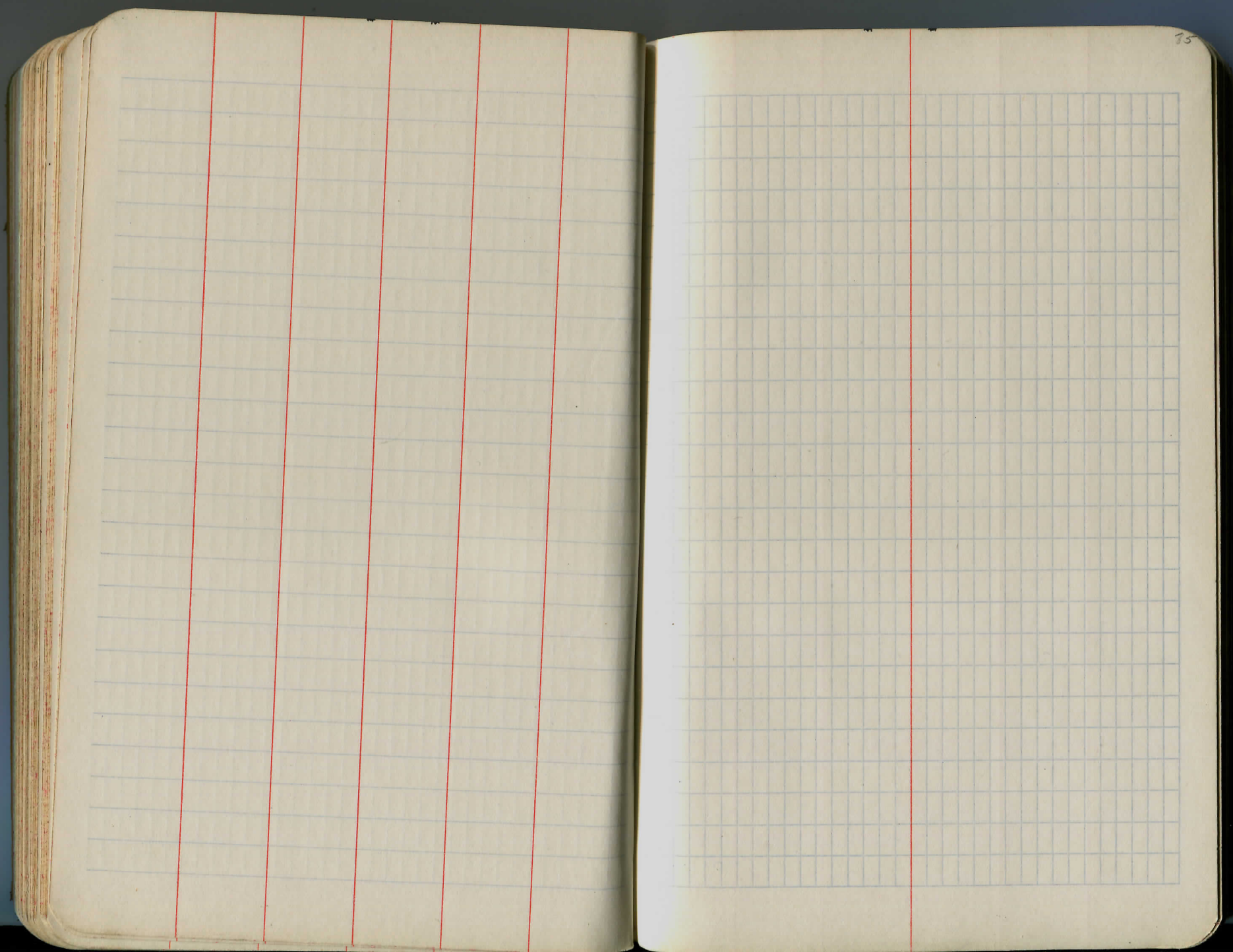


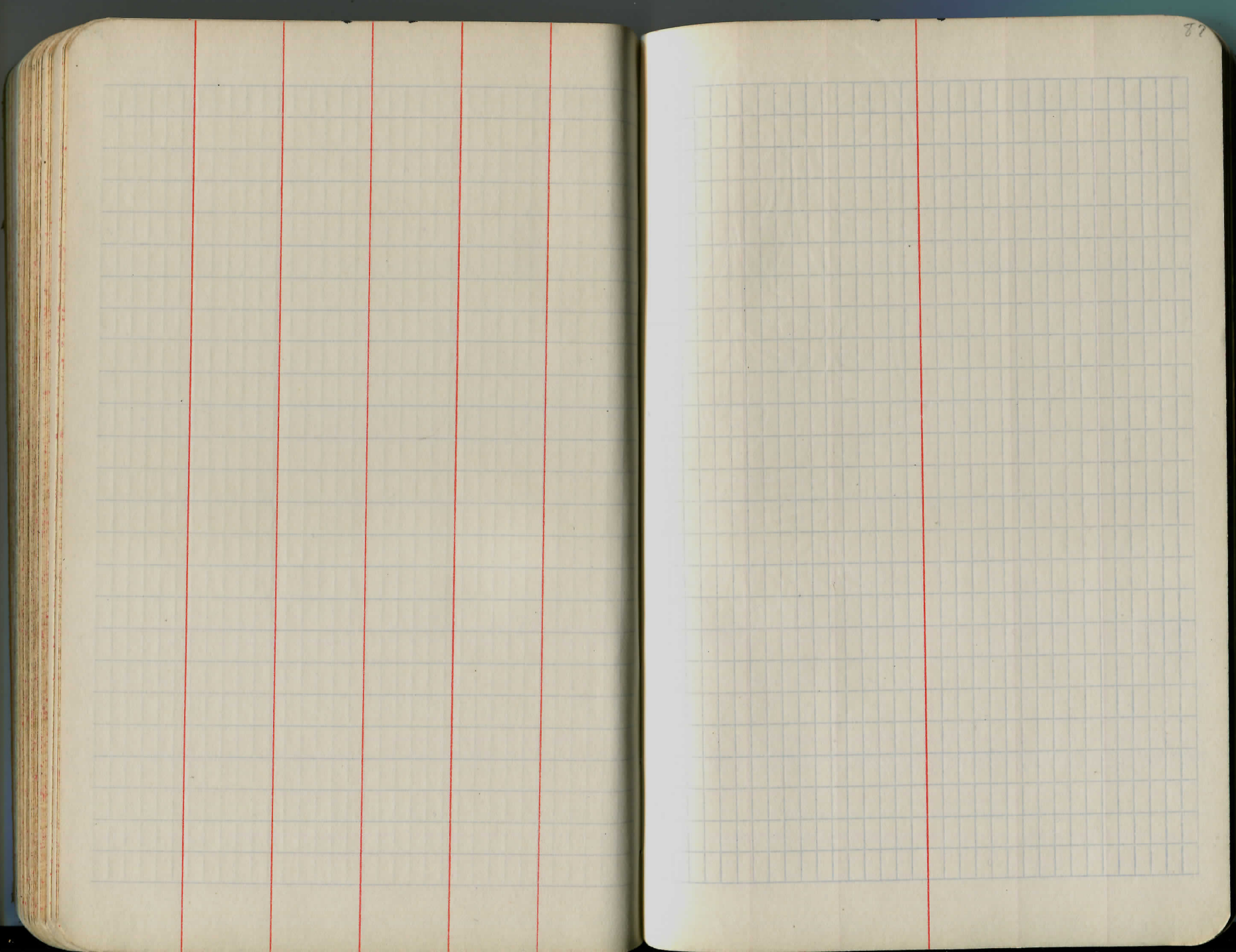


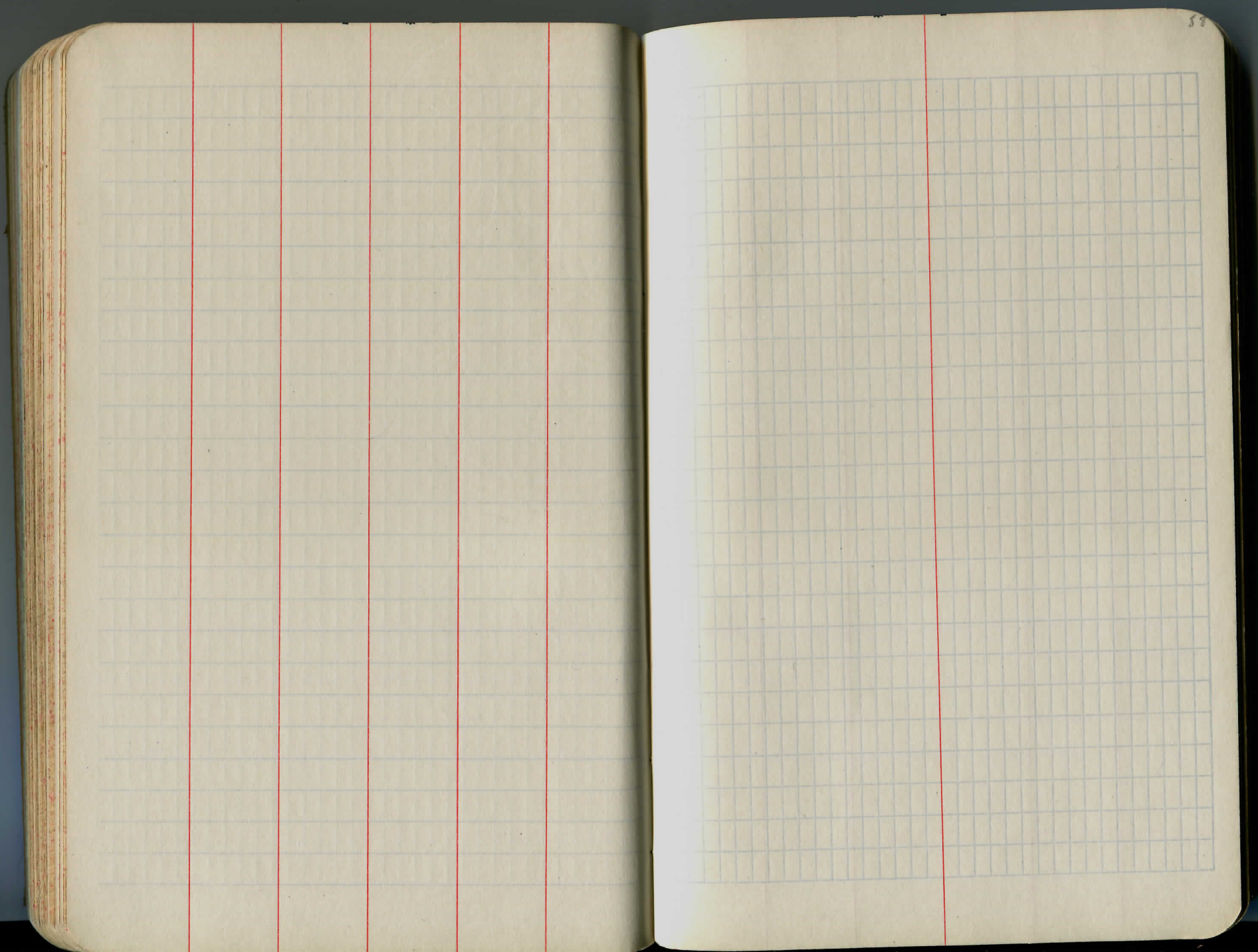


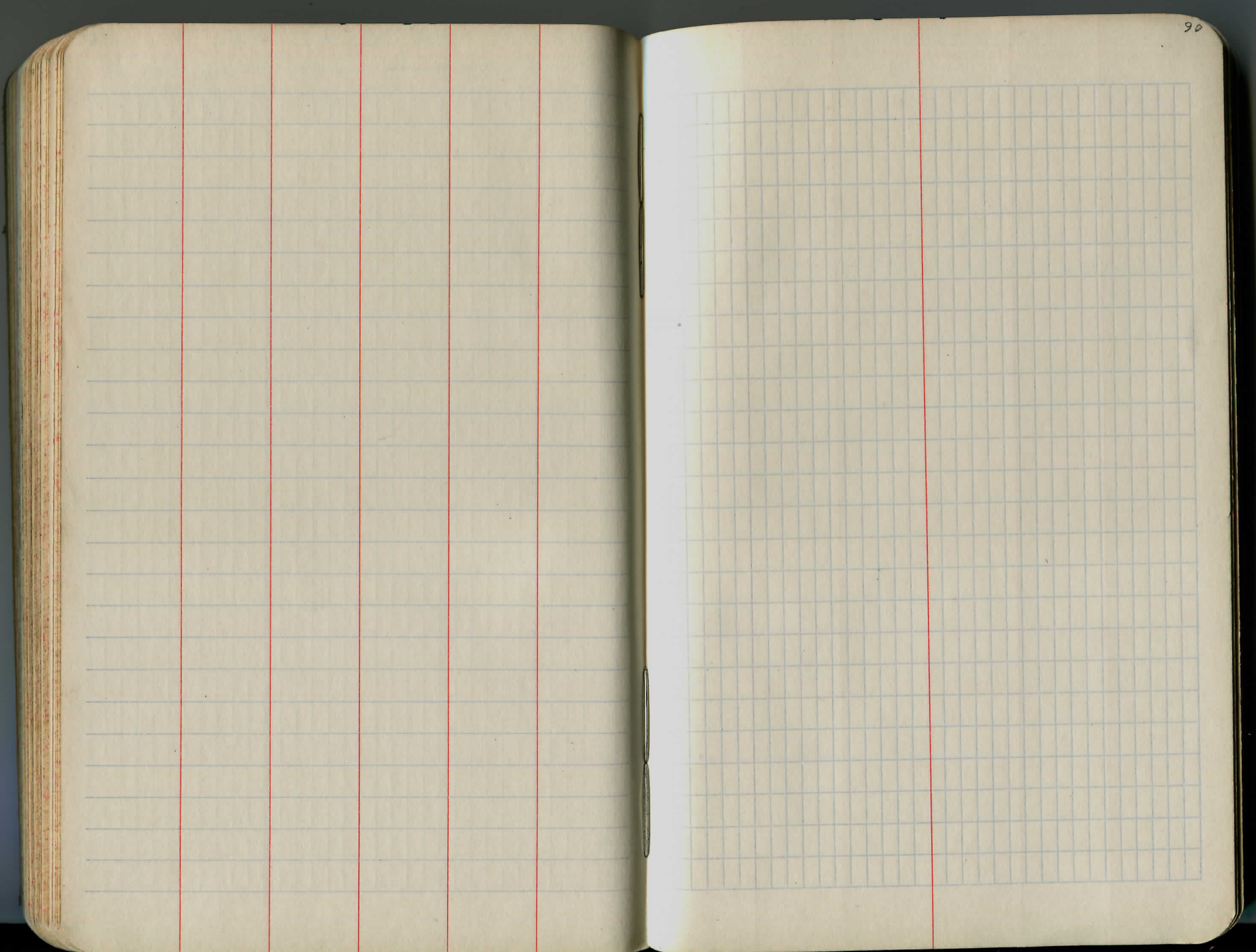




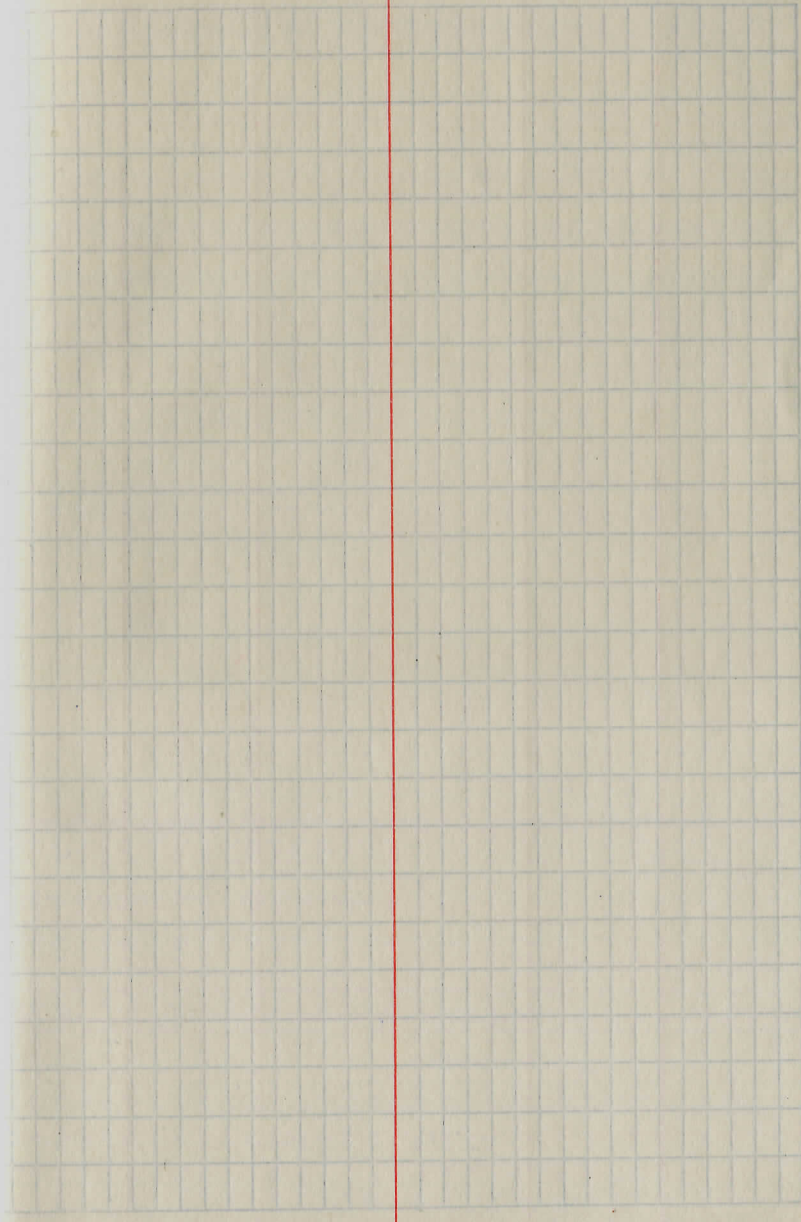
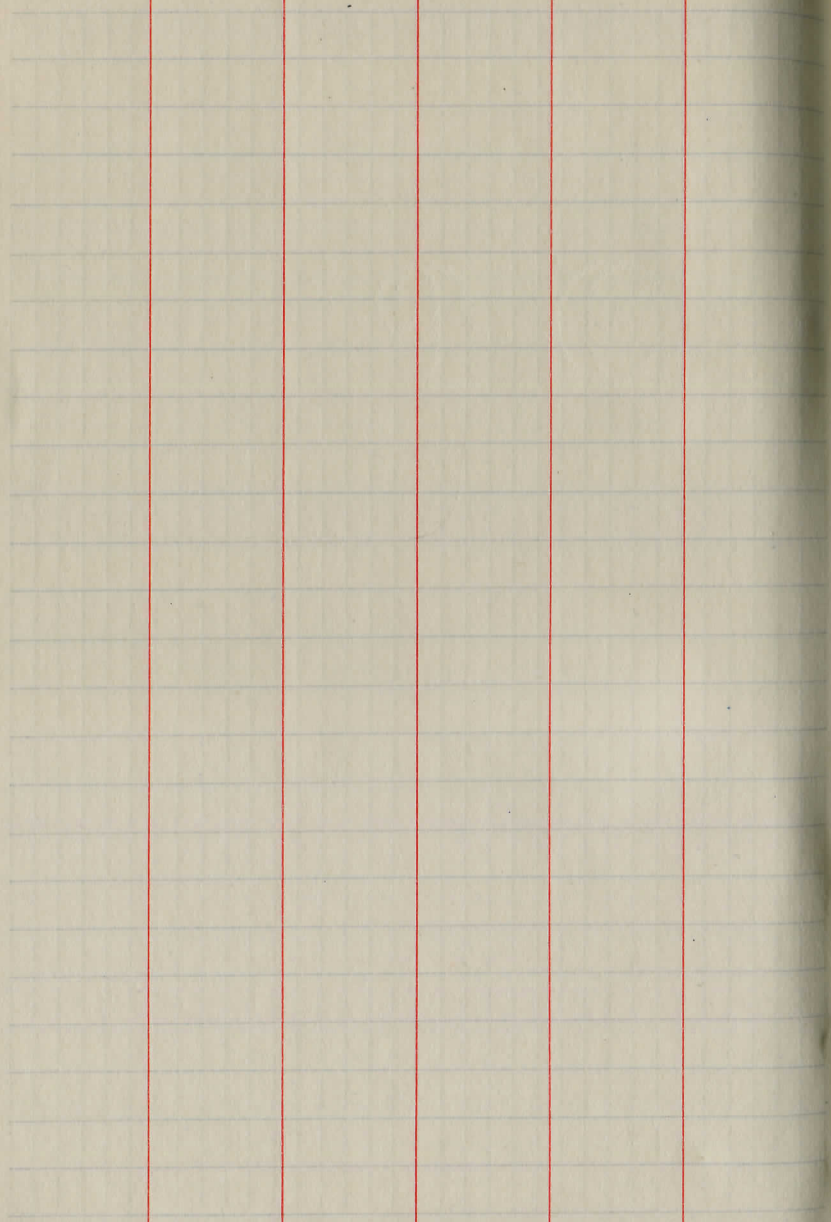


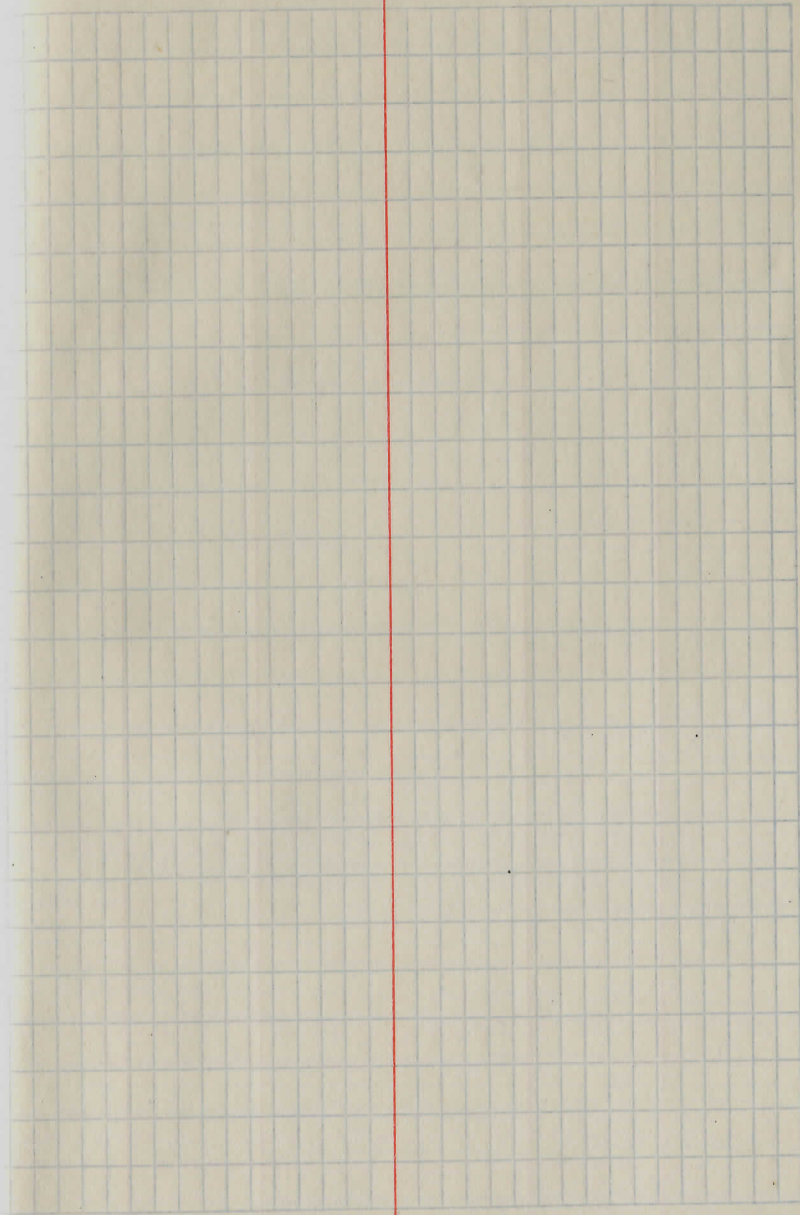
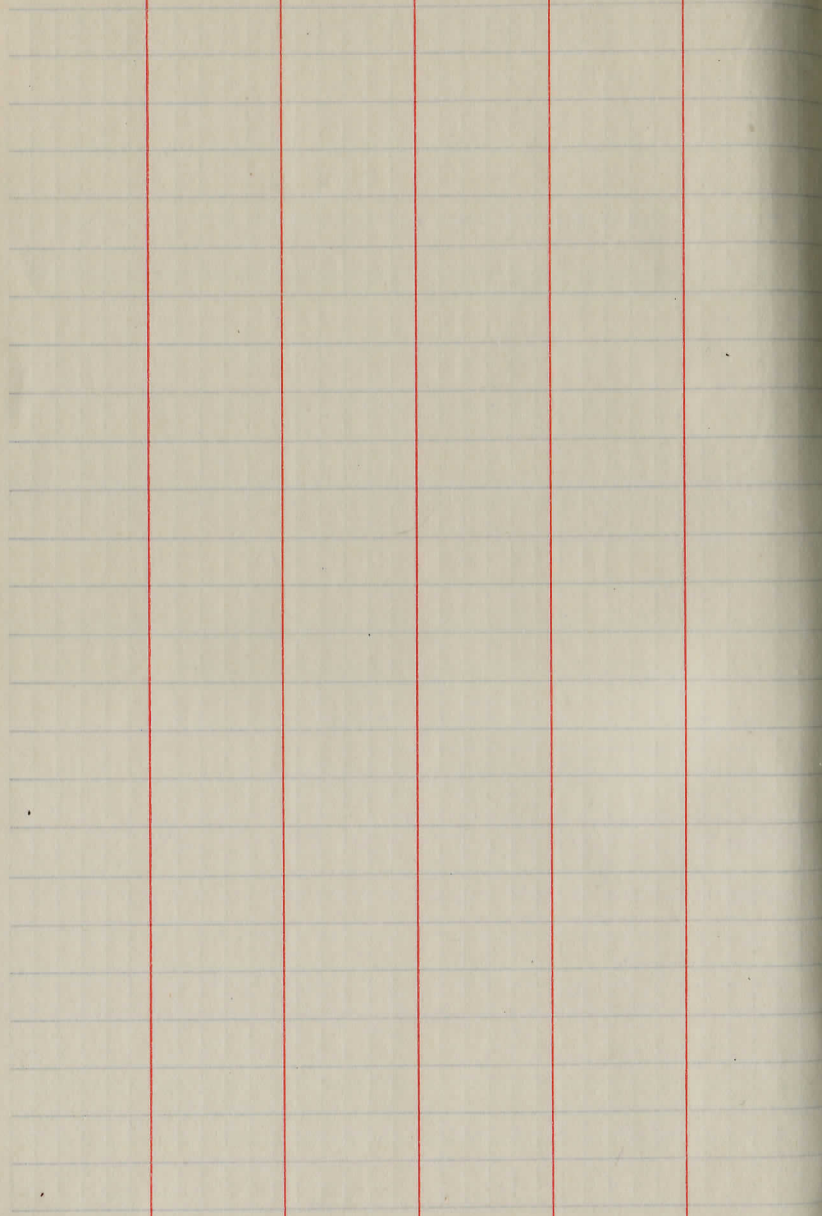


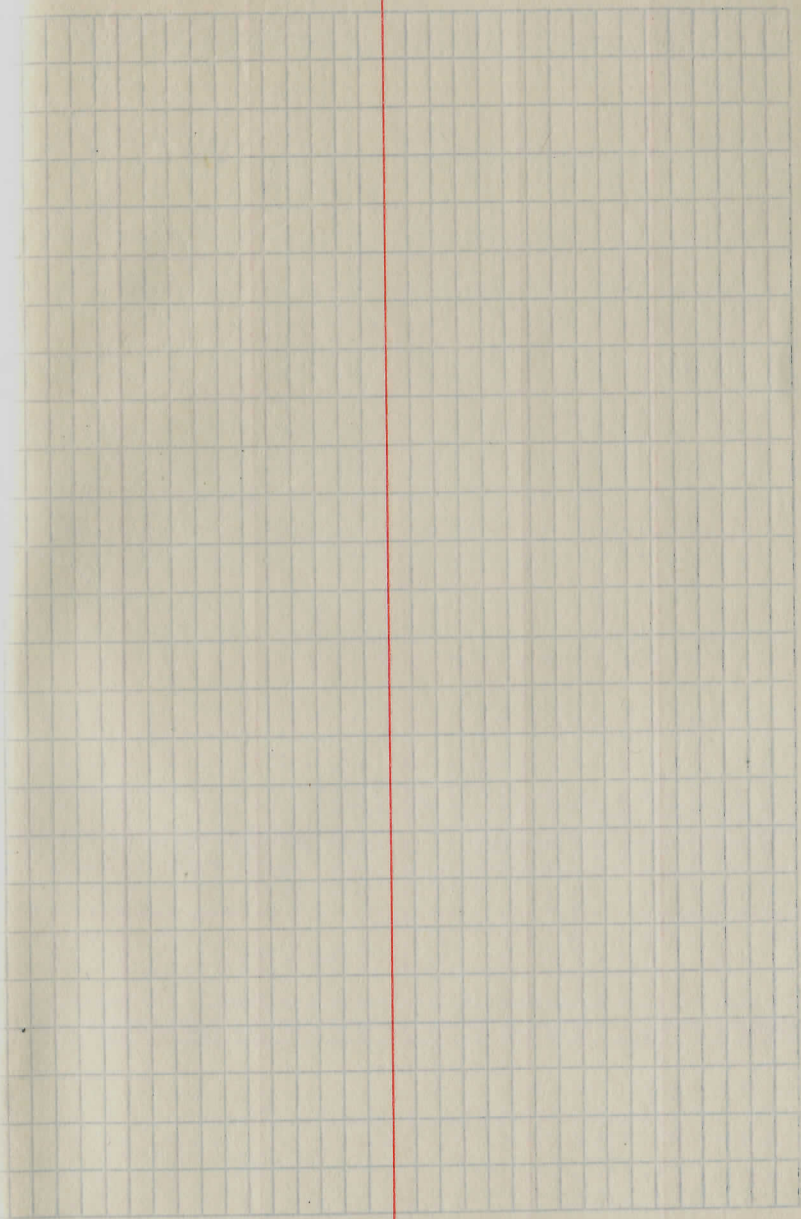
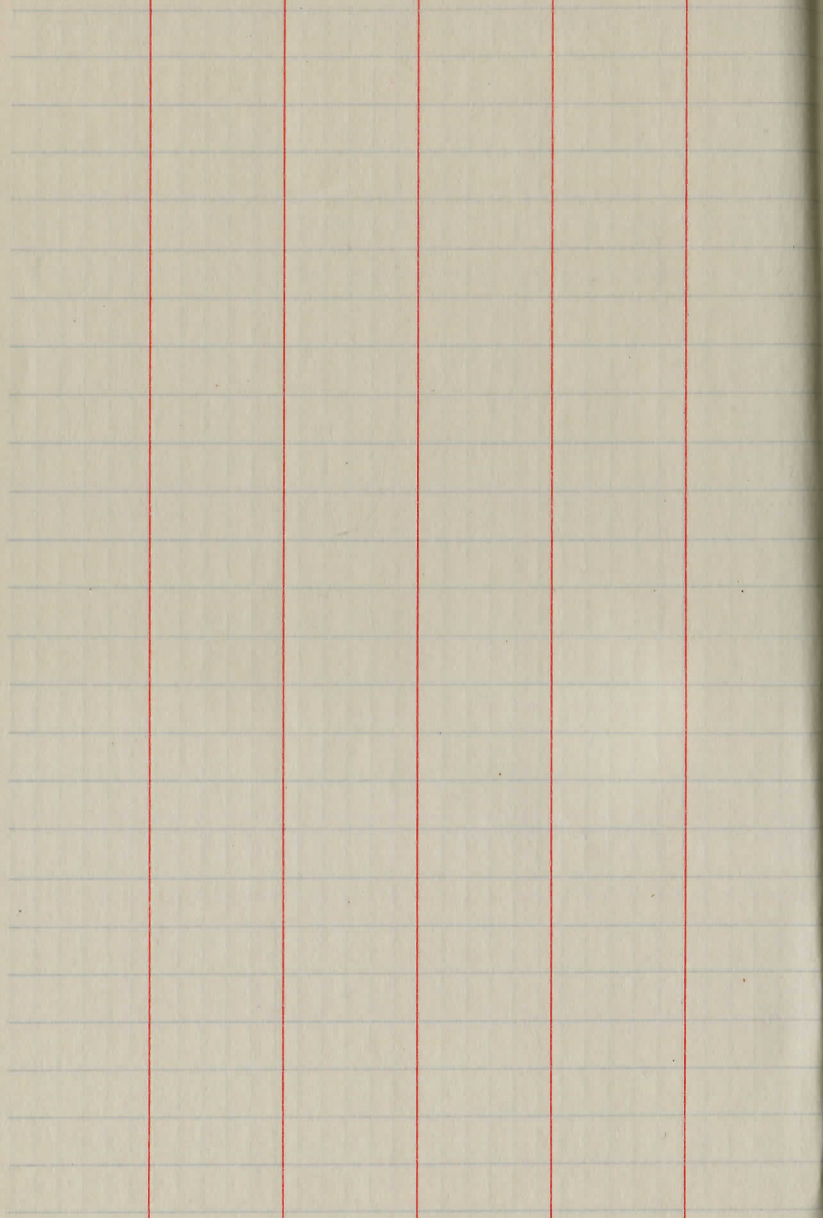




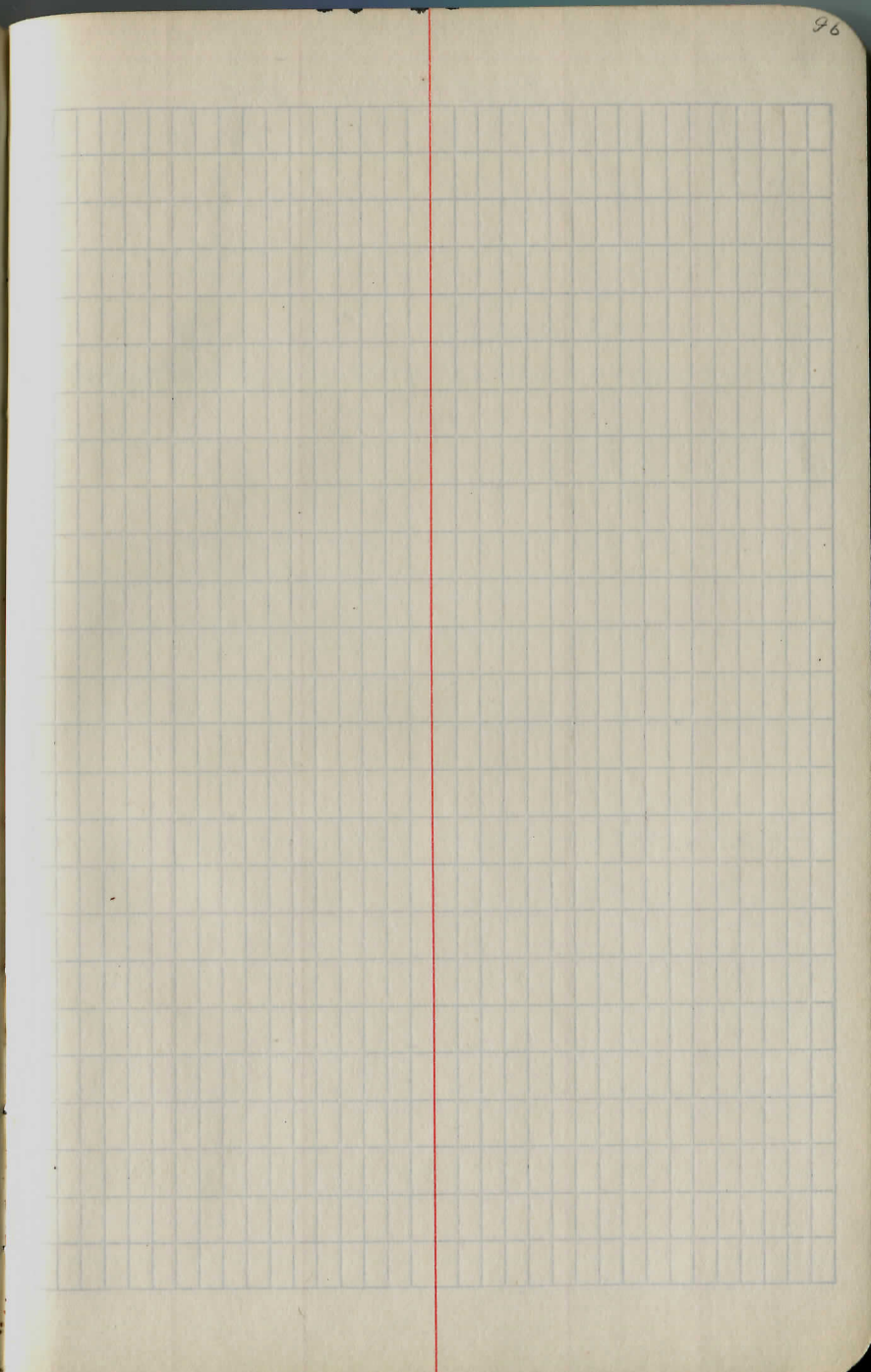
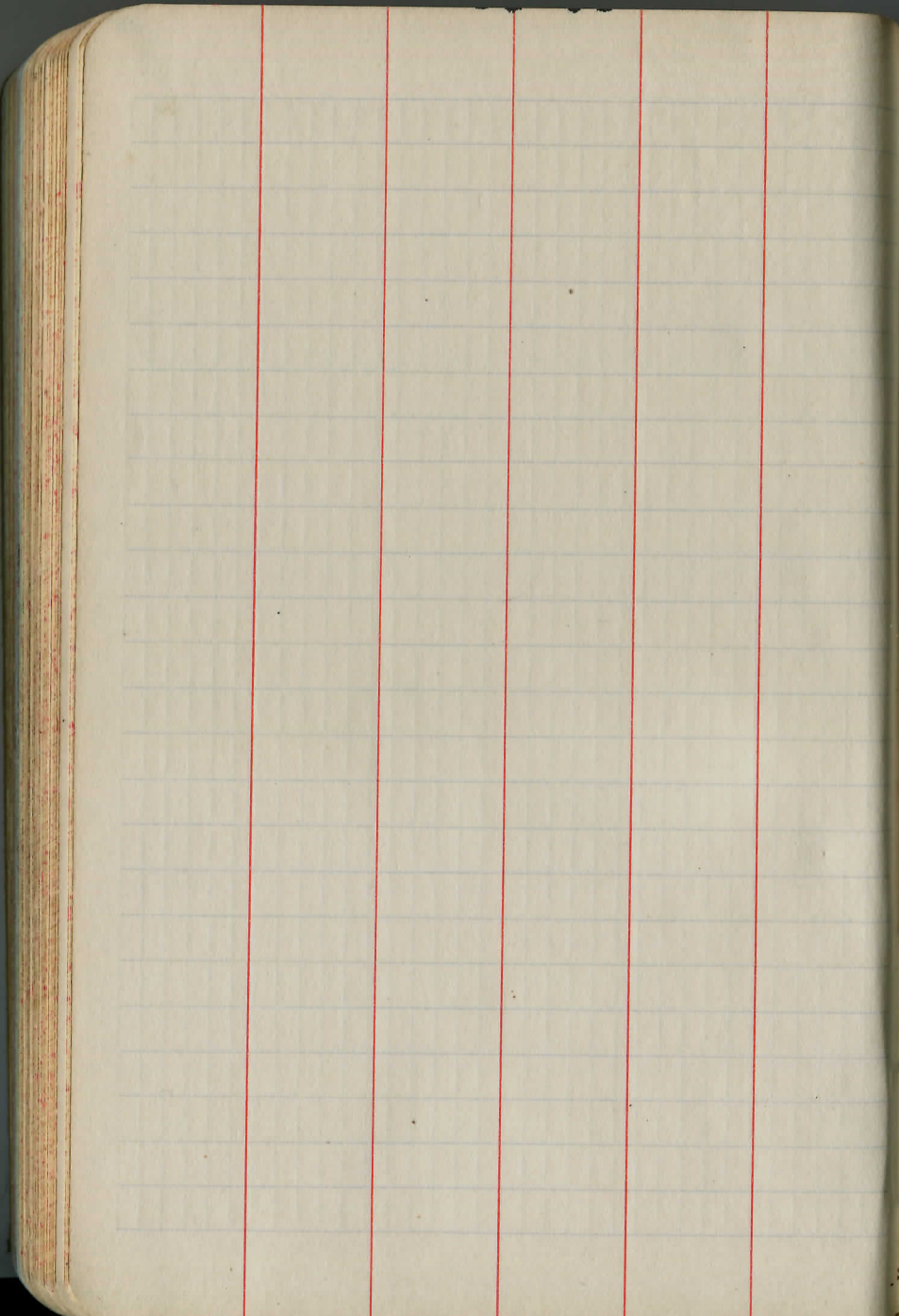


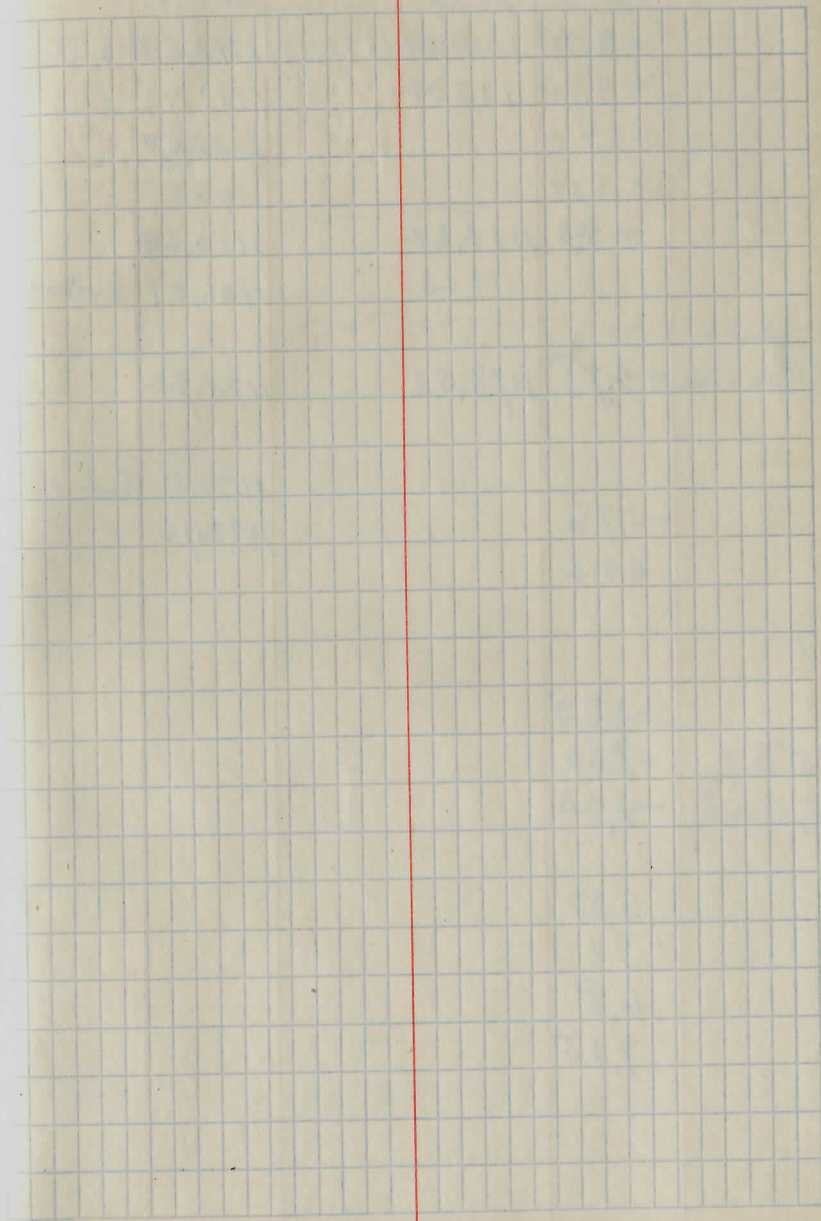






The image shows an open notebook with two pages. The left page is ruled with a grid of light blue lines and features five vertical red lines that divide the page into six columns. The right page is also ruled with a grid of light blue lines and features one vertical red line on the left side, creating two columns. The number '95' is handwritten in the top right corner of the right page. The notebook's binding is visible on the left edge.





	NO	Nov,
-3.70	1114.04	1110.64 8 stamps
+4.70	1115.34	
G 8.74		1106.50
G 8.37		1106.97
+4.0	1114.64	1110.64
	8.43	1106.21 & Real

7-13-32

T. P. on stone +4.78 1178.52

1173.74

-5.76

602

1171.5 Ends of gutter  
1172.76

56

+350

75° S. E. -860

& Real -440

6.30

7.1

6.8

7.15

35-

5-7  
3  
1/2

98

Kinkler & Barton June 22<sup>nd</sup> 1932  
 Trustees Sidley - Coe & Logget  
 B.N.J. #5 + 0.75 1119.94  
 9.84  
 T.P. #756 -9.20 1110.74  
 + 804 1118.78 GR 6.54 1112.24  
 W. end 12" tile line R. 1.04 stake -  
 GR 7.04 1111.74 W. end  
 R. 3.04 stake cut 4.0 ft.  
 Top of bridg #7+56 1112.06

Length of Ditch " " " from peg (1110.74)  
 To 33+54 along ditch 158.5 ft. - 0.126  
 Ditch 47+56 to Taylor W. line 831 ft.

7-6-32

P.M.	+ 4.20	1114.62	1110.42	8" Elm	
E Rd. at	x.0	-5.00	1109.62	31+40	
culvert		7.00	1107.6	Right	
Location		7.20	1107.4	Left	
1st Curve		7.70			
radius	70±				
	+ 1.85	1112.27	1110.42	grade-fl.	
End = 0	at ang to SE	8.10	1104.17	1104.17	
1	c. 0.5	7.40	1104.9	1104.44	
2	+ 0.27%	c. 0.6	7.00	1105.3	1104.71
3		c. 0.7	6.60	1105.7	1104.98
4		c. 0.5	6.20	1106.1	1105.25
5		c. 2.5	4.20	1108.1	1105.52
6		c. 3.0	3.50	1108.8	1105.99

	276	
	1119.19	
- 49	1119.95	11014
	1110.2	1104.17
	9.75	6
		1100.17

116+90: 25' Lt. spike in NE root 26"  
maple 1142.82

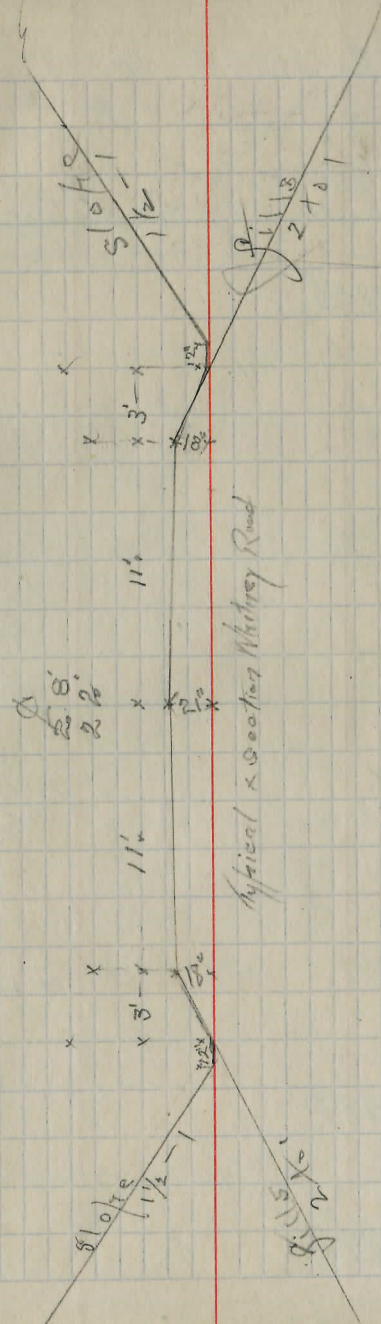
1st corner E. of road to N. on S. side Rd  
& " obt. S Ma. 116.

155+05: 50' Rt. spike in W. 12" W. Cherry  
1243.19 - Whitney  
Road intersects Sta 156.

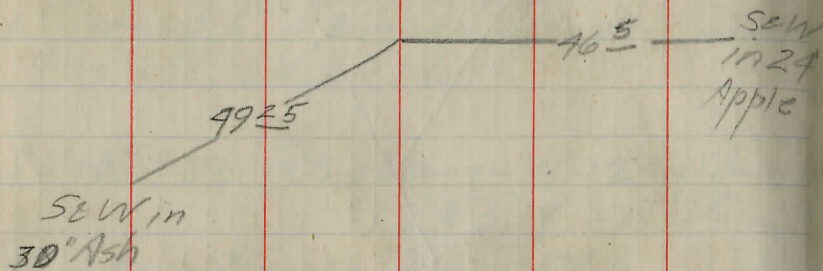
144+12: 25' 1/2 R. spike in W. root 15"  
142+58.5 = P.C. to Lt. (Rhodes to W.)  
1216.93

(preexisting loc)	AD	Elv.
34+78 ± 1/2 of 24" culvert 40 long on skew with road		
-6.02	1115.64	1109.62
Sta 7 (e. road)	6.3	c. 3.20 1109.3 1106.06
7+57 8	5.45	c. 3.9 > 1109.62 1106.121
9	4.95	c. 4.1 1110.7 1106.60
10	4.95	c. 3.8 1110.7 1106.87
+55	6.80	c. 1.8 1108.8 <sup>angle in</sup> <sub>between</sub>
	+0.63	1186.98 BM # 10
road over Estimation	-8.70	1178.91 (?)
T.P. on stone	-13.87	1173.74
Header in detail line		

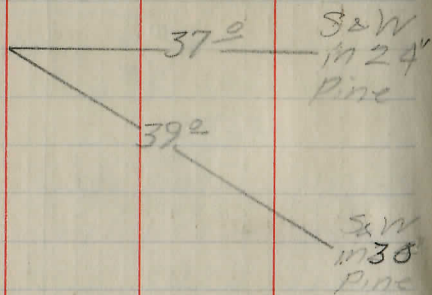
.27  
100  
55  
135  
105  
1785



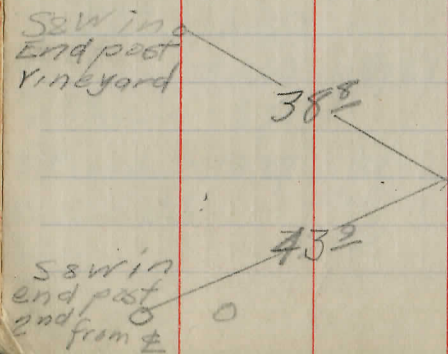
Ref to PI 1000' N X Rd



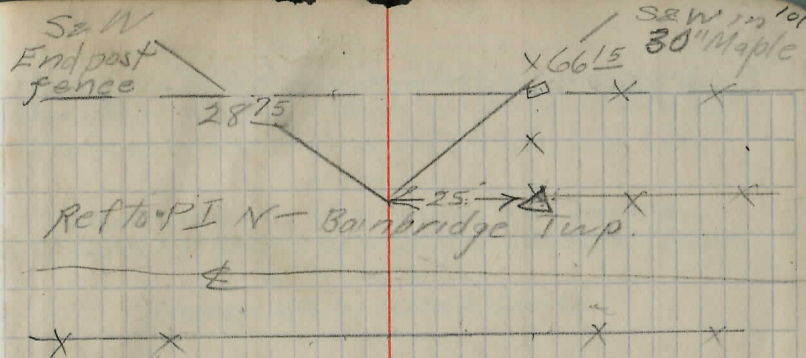
Ref to PI 600' N of Main Market



Ref to POT 500' S of Twp Line



SEW End post fence



Sec. 7204 - Obstructions to highways

# KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

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## HOW TO USE KEITH'S TABLES.

### EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle  
of Intersection or I. P. =  $23^{\circ} 20'$  to the R. at Station  
542+72.

Ext. in Tab. IV opposite  $23^{\circ} 20' = 120.87$   
 $120.87 \div 12 = 10.07$ . Say a  $10^{\circ}$  Curve.

Tan. in Tab. IV opp.  $23^{\circ} 20' = 1183.1$   
 $1183.1 \div 10 = 118.31$ .

Tab. V. correction for A.  $23^{\circ} 20'$  for a  $10^{\circ}$  Cur. = 0.16  
 $118.31 + 0.16 = 118.47 =$  corrected Tangent.

(If corrected Ext. is required find in same way)  
Ang.  $23^{\circ} 20' = 23.33^{\circ} \div 10 = 2.3333 =$  L. C.

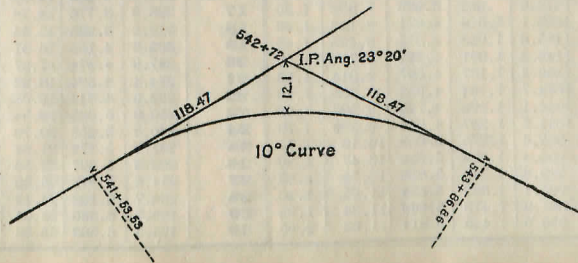
$2^{\circ} 19\frac{1}{2}' =$ def. for sta. 542	I. P. = sta.	542+72
$4^{\circ} 49\frac{1}{2}' =$ " " " +50	Tan. =	1.18.47
$7^{\circ} 19\frac{1}{2}' =$ " " " 543	B. C. = sta.	541+53.53
$9^{\circ} 49\frac{1}{2}' =$ " " " +50	L. C. =	2.33.33
$11^{\circ} 40' =$ " " " 543+	E. C. = sta.	543+86.86
86.86		

$100 - 53.53 = 46.47 \times 3' (\text{def. for 1 ft. of } 10^{\circ} \text{ Cur.}) = 139.41' =$   
 $2^{\circ} 19\frac{1}{2}'' =$  def. for sta. 542.

Def. for 50 ft. =  $2^{\circ} 30'$  for a  $10^{\circ}$  Curve.

Def. for 36.86 ft. =  $1^{\circ} 50\frac{1}{2}'$  for a  $10^{\circ}$  Curve

(These tables are published in Field Books of  
KEUFFEL & ESSER Co., New York, N. Y.)



70 + 42.4  
42.2  
38.20  
29.15  
64.33

57.50 60

9.75 R  
29.62  
48.99

139.46  
27 - 37

45.33  
123 09.20  
36.03

122 + 09  
106 104  
16 05  
99 15  
66 + 54  
32 61

24 00.00  
2295.82  
104.18

17022.33  
1418.65  
15603.68

6.70

PLEASE RETURN TO  
GEAUGA COUNTY ENGINEER  
COURT HOUSE  
CHARDON, O.  
PHONE 250-X

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. (SEE STUPEPS 1 TO 1.)

FOR SINGLE TRACK TRACKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17							32.4	33.6	33.7	33.9	17
18							34.9	35.1	35.2	35.4	18
19							36.4	36.6	36.7	36.9	19
20							37.9	38.1	38.2	38.4	20
21							39.4	39.6	39.7	39.9	21
22							40.9	41.1	41.2	41.4	22
23							42.4	42.6	42.7	42.9	23
24							43.9	44.1	44.2	44.4	24
25							45.4	45.6	45.7	45.9	25
26							46.9	47.1	47.2	47.4	26
27							48.4	48.6	48.7	48.9	27
28							49.9	50.1	50.2	50.4	28
29							51.4	51.6	51.7	51.9	29
30							52.9	53.1	53.2	53.4	30
31							54.4	54.6	54.7	54.9	31
32							55.9	56.1	56.2	56.4	32
33							57.4	57.6	57.7	57.9	33
34							58.9	59.1	59.2	59.4	34
35							60.4	60.6	60.7	60.9	35
36							61.9	62.1	62.2	62.4	36

LEGAL NOTICE

In the matter of the improvement of Whitney, in Montville township. Notice is hereby given that a resolution has been adopted providing for said improvement by the Board of Trustees of said township, Geauga County, Ohio, and that copies of the surveys, plans, profiles, cross-sections, estimates, specifications for said improvement are on file with the said township trustees for the inspection and examination of all persons interested therein.

That on the 3rd day of September, 1932, at 8:00 o'clock p. m. in the Town Hall in said township, is the time and place for hearing objections to said improvement and for hearing claims for compensations for lands and property to be taken for said improvement, or damages sustained on account thereof, and that unless such claims are filed in writing with the said township trustees on or before the time fixed therein for hearing said claims, the same shall be waived except as to minors and other persons under disability.

L. E. RHODES,  
Clerk of the Board of  
Township Trustees of  
Montville Township.

m. Soc. C. E.

MADE IN GERMANY.

R.

LEGAL NOTICE

33-34

1450